

Text No.24

**COMBUSTION TECHNOLOGIES  
FOR ENERGY CONSERVATION**

**省エネルギーのための燃焼技術**

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サーモシステム・カンパニー技術部部長

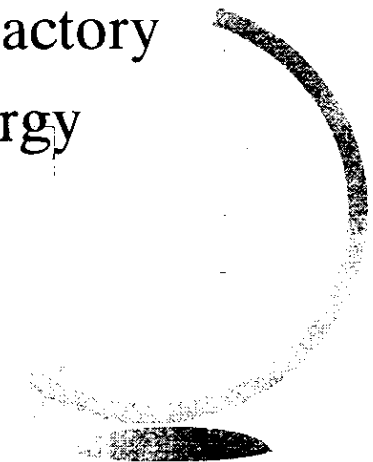
# Schedule

## Chapter 1

- ✧ Combustion & Flame
- ✧ Fuel Type
- ✧ Classification of Burner
- ✧ New Combustion Technology
- ✧ Combustion Technology for Energy Saving and Low Environmental Pollution

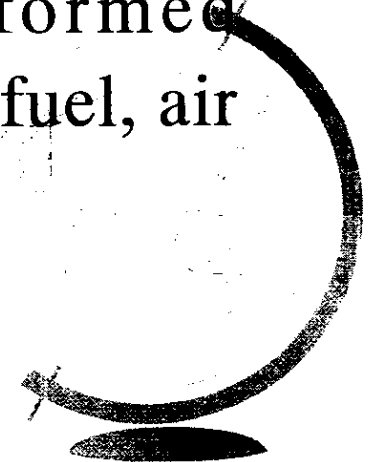
## Chapter 2

- ✧ Decomposition of Burners
- ✧ Industrial Furnace Conservation Techniques
  - Furnace Pressure
  - Furnace Design
- ✧ Explanation of the Furnace in ECCJ Model Factory
- ✧ How to Save Energy



# Definition of Combustion and Flame

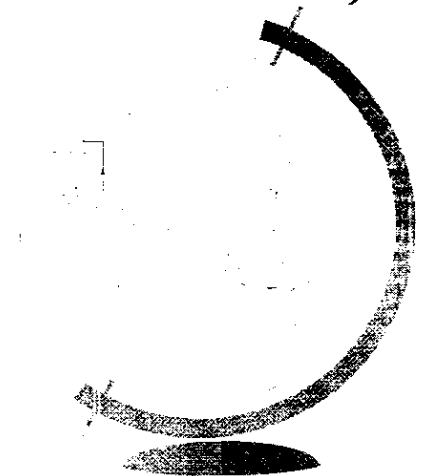
- ◆ Combustion is defined as the process which changes the chemical energy of fuel to the thermal energy by oxidizing reaction with oxidant like air, which rapid heat and visible ray release is accompanied.
- ◆ Flame is the state of gas phase and formed generally in the flow region of mixture of fuel, air and burning products.



# Fuel Type (1) --- Gas Fuel

- ◆ High Combustion Efficiency
- ◆ Firing Low Excess Air Ratio
- ◆ Easy Combustion Control
- ◆ Usually No Sulfur Content ( No SO<sub>x</sub> Emission )
- ◆ Typical Gas Fuel

LNG, LPG, COG, Hydrogen, etc



-4-

Name	Component %									Density kg/m <sup>3</sup> N	Low Calorific Value MJ/m <sup>3</sup> N	Theoretical Air Requirement m <sup>3</sup> N/m <sup>3</sup> N	Theoretical Combustion Product m <sup>3</sup> N/m <sup>3</sup> N		
	CO <sub>2</sub>	CO	CH <sub>4</sub>	C <sub>3</sub> H <sub>8</sub>	C <sub>4</sub> H <sub>10</sub>	C <sub>m</sub> H <sub>n</sub>	H <sub>2</sub>	O <sub>2</sub>	N <sub>2</sub>				CO <sub>2</sub>	H <sub>2</sub> O	N <sub>2</sub>
Butane Gas	0	0	0	0	100	0	0	0	0	2.593	118.6	31.09	4.00	5.00	24.59
Propane Gas	0	0	0	100	0	0	0	0	0	1.967	91.3	23.91	3.00	4.00	18.91
Natural Gas	0	0	89.8	2.9	1.4	C <sub>2</sub> H <sub>6</sub> 5.9	0	0	0	0.815	40.2	10.66	1.15	2.16	8.42
City Gas (13A)	0	0	88.0	4.0	2.0	C <sub>2</sub> H <sub>6</sub> 6.0	0	0	0	0.841	41.7	11.00	1.20	2.20	8.65
City Gas (6A)	0	0	0	1.0	21.1	0	0	16.4	61.5	1.570	27.1	5.80	0.84	1.06	5.18
COG	3.0	7.0	27.0	0	4.0	0	57.0	0.5	1.5	0.467	19.1	4.74	0.45	1.19	3.72
BFG	21.1	22.0	0	0	0	0	2.8	0	54.1	1.367	3.0	0.59	0.43	0.03	1.01

**Table 1. Properties of Gas Fuel**

## Fuel Type (2) --- Liquid Fuel

- ◆ Relatively Cheaper than Gas Fuel
- ◆ Easy to Handle and Transport
- ◆ Uniform Calorific Value ( 10000 kcal/kg )
- ◆ Necessity of Sulfur and Ash Treatment
- ◆ Necessity of Heating up ( Fuel Oil Type2&3)
- ◆ Typical Liquid Fuel

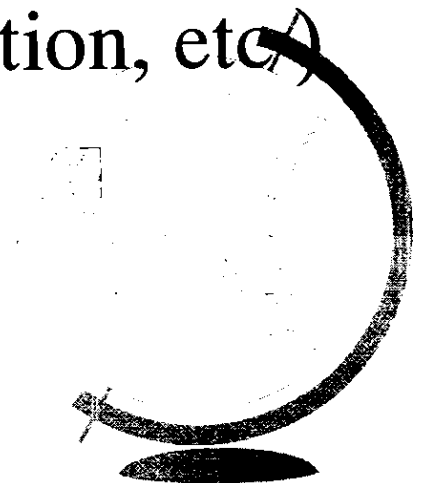
Kerosene, Light Oil, Fuel Oil Type1 etc.

Name	Component wt %							Density g/cm <sup>3</sup>	kinematic Viscosity mm <sup>2</sup> /s	Low Calorific Value MJ/kg	Theoretical Air Requirement m <sup>3</sup> N/kg	Theoretical Combustion Product m <sup>3</sup> N/kg			
	C	H	O	N	S	H <sub>2</sub> O	Ash					CO <sub>2</sub>	H <sub>2</sub> O	SO <sub>2</sub>	N <sub>2</sub>
Kerosene	85.7	14.0	0	0	0.5	0	0	0.78~0.83	2	43.5	11.40	1.59	1.56	0.00	9.02
Light Oil (Diesel Oil)	85.9	13.6	0	0	0.5	0	0	0.81~0.84	4	43.0	11.20	1.60	1.51	0.00	8.87
Fuel Oil Type 1	85.9	12.0	0.7	0.5	0.5	0.3	0.05	0.85~0.88	~50	42.7	10.90	1.60	1.34	0.00	8.61
Fuel Oil Type 2	84.5	11.3	0.4	0.4	3.0	0.4	0.05	0.90~0.93	~150	41.3	10.70	1.58	1.27	0.02	8.44
Fuel Oil Type 3	84.0	10.9	0.5	0.4	3.5	0.5	0.10	0.93~0.95	< 1000	41.4	10.50	1.57	1.21	0.02	8.27
Gasoline	85.0	15.0	0	0	0	0	0	0.70~0.74	> 1	44.1	11.60	1.59	1.68	0.00	9.18

Table 2. Properties of Liquid Fuel

## Fuel Type (3) --- Solid Fuel

- ◆ Difficult to Handle and Transport
- ◆ Relatively Cheaper than Gas and Liquid Fuel
- ◆ Necessity of Sulfur and Ash Treatment
- ◆ Necessity of Pretreatment  
( Crushing, Gasification, Liquefaction, etc )
- ◆ Typical Solid Fuel  
Coal ( Many Types ), Cokes, etc





Name	Component wt %							True Specific Gravity g/cm <sup>3</sup>	Low Calorific Value MJ/kg	Theoretical Air Requirement m <sup>3</sup> N/kg	Theoretical Combustion Product m <sup>3</sup> N/kg			
	C	H	O	N	S	H <sub>2</sub> O	Ash				CO <sub>2</sub>	H <sub>2</sub> O	SO <sub>2</sub>	N <sub>2</sub>
Foundry Coke	85.5	0.3	0.1	0	0.5	0.3	12.6	1.8~2.0	28.9	7.75	1.61	0.03	0.00	6.09
Iron-making Coke	79.4	0.4	0	0	0.6	0.8	18.4	1.8~1.9	27.0	7.21	1.49	0.05	0.00	5.66
Gas Coke	75.7	0.4	0.8	0	1.1	3.9	19.8	~1.8	26.1	6.73	1.39	0.09	0.01	5.29
Peat	21.0	6.3	62.9	1.1	0.6	0	6.0		5.5	1.51	0.40	0.72	0.00	1.20
Brown Coal	42.4	6.6	42.1	0.6	1.1	0	7.2		16.1	4.16	0.79	0.74	0.01	3.28
Bituminous Coal	78.0	5.2	7.5	1.3	1.0	0	7.1	1.25~1.45	32.1	8.11	1.46	0.59	0.01	6.38
Anthracite	84.4	1.9	4.4	0.6	0.9	0	7.8	1.3~1.8	30.3	7.89	1.58	0.22	0.01	6.20

**Table 3. Properties of Solid Fuel**

# Classification of Burner

- ◆ Type of Draft

  - Natural Draft & Forced Draft

- ◆ Heating Method

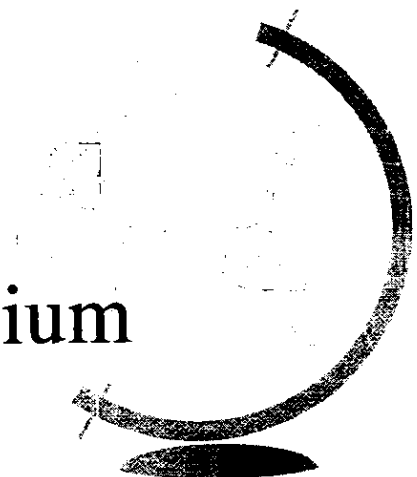
  - Direct & Indirect Heating

- ◆ Air / Fuel Mixing Method

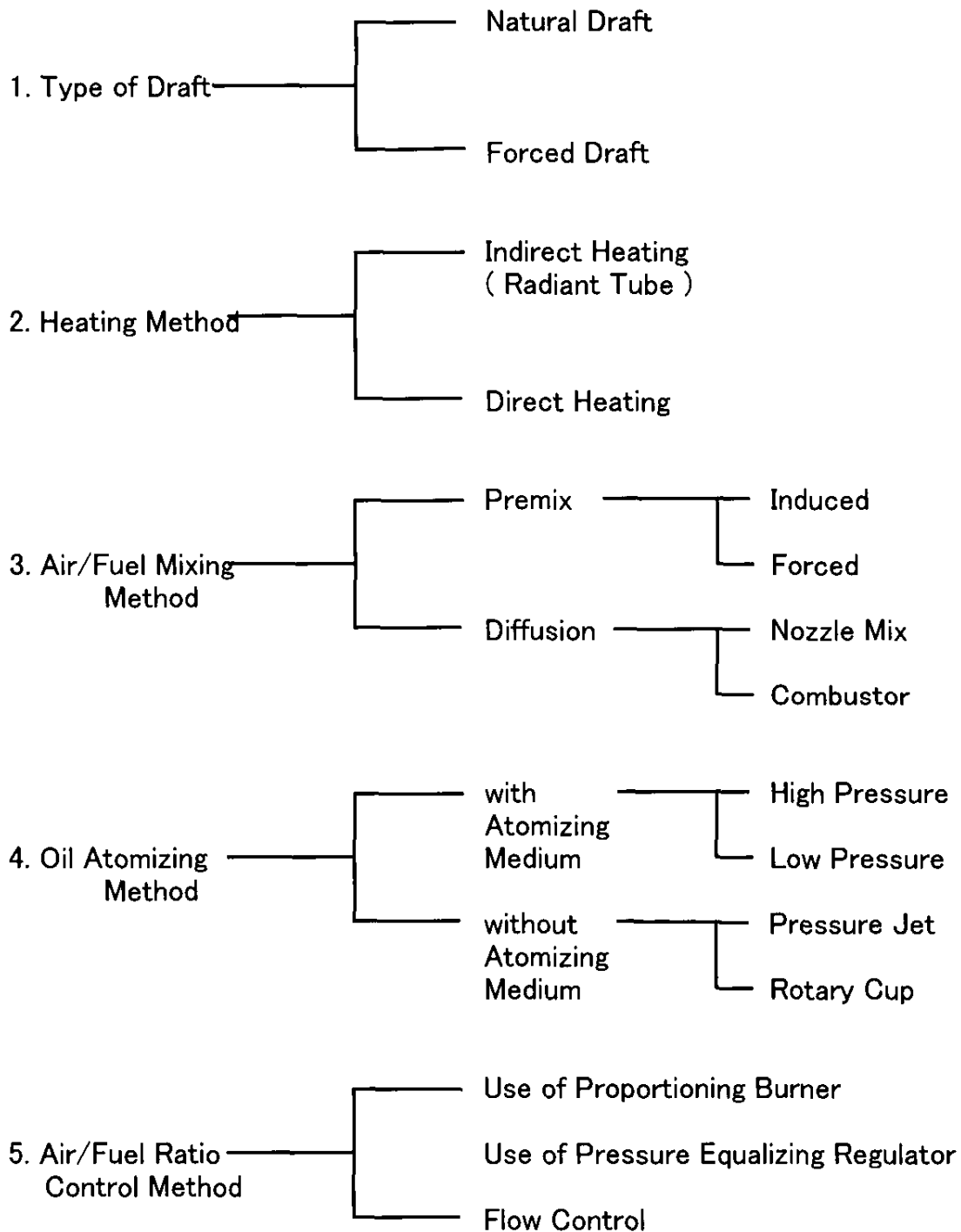
  - Premix & Diffusion Mixing

- ◆ Oil Atomising Method

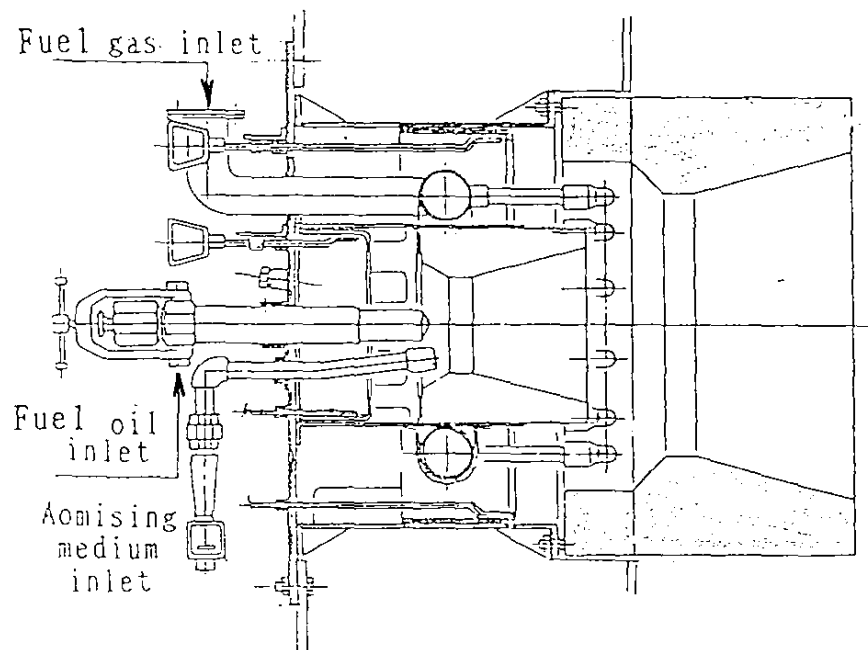
  - With & Without Atomising Medium



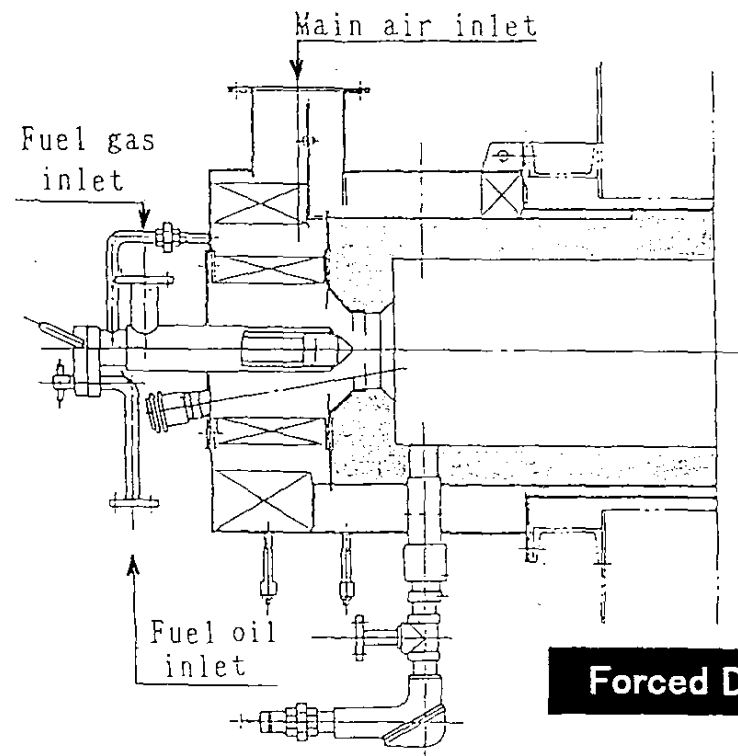
# Classification of Industrial Burners



## Classification by Type of Draft



**Natural Draft**



**Forced Draft**

Vortometric oil/gas combination burner (Model:CVS)

Oil/gas combination burner (Model:PCMG)

Air/fuel ratio : 1.3~1.5

Preheated air : not used

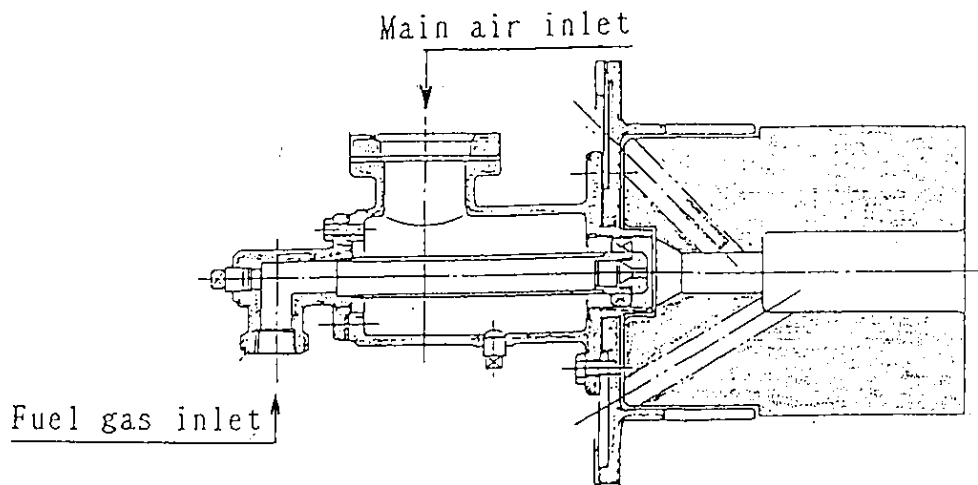
Turndown : 1:4

Air/fuel ratio : 1.05~1.1

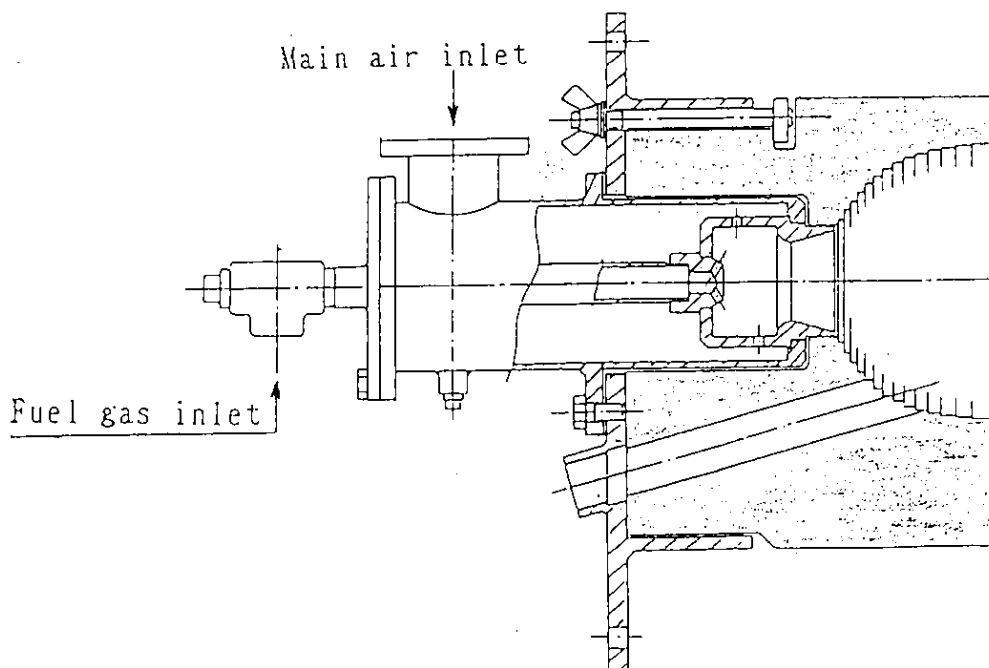
Preheated air : to be used

Turndown : 1:10

## Classification by Heating Method Direct

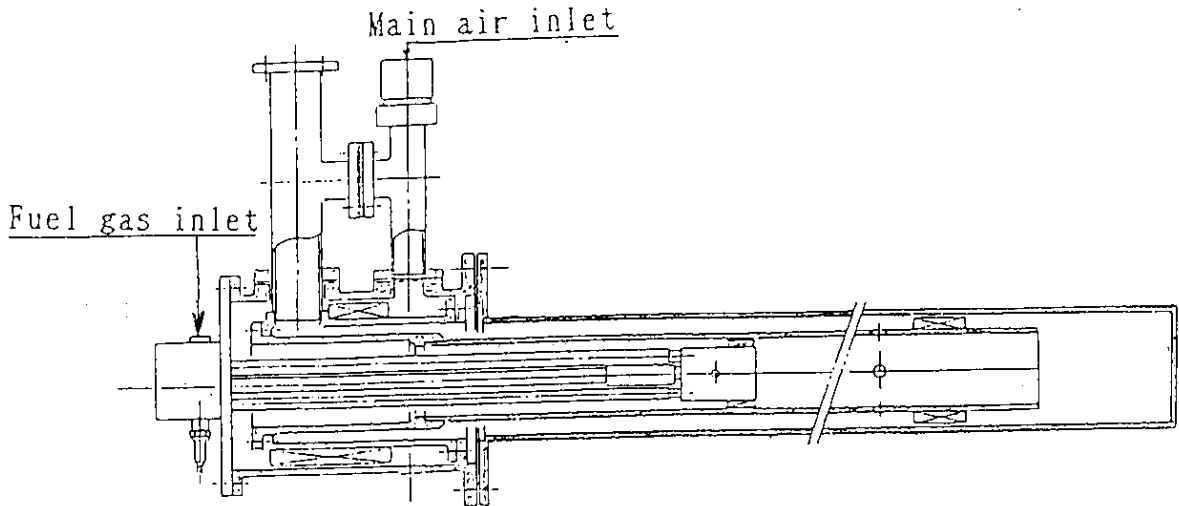


Convection heating  
High momentum gas burner (Model:HMG)

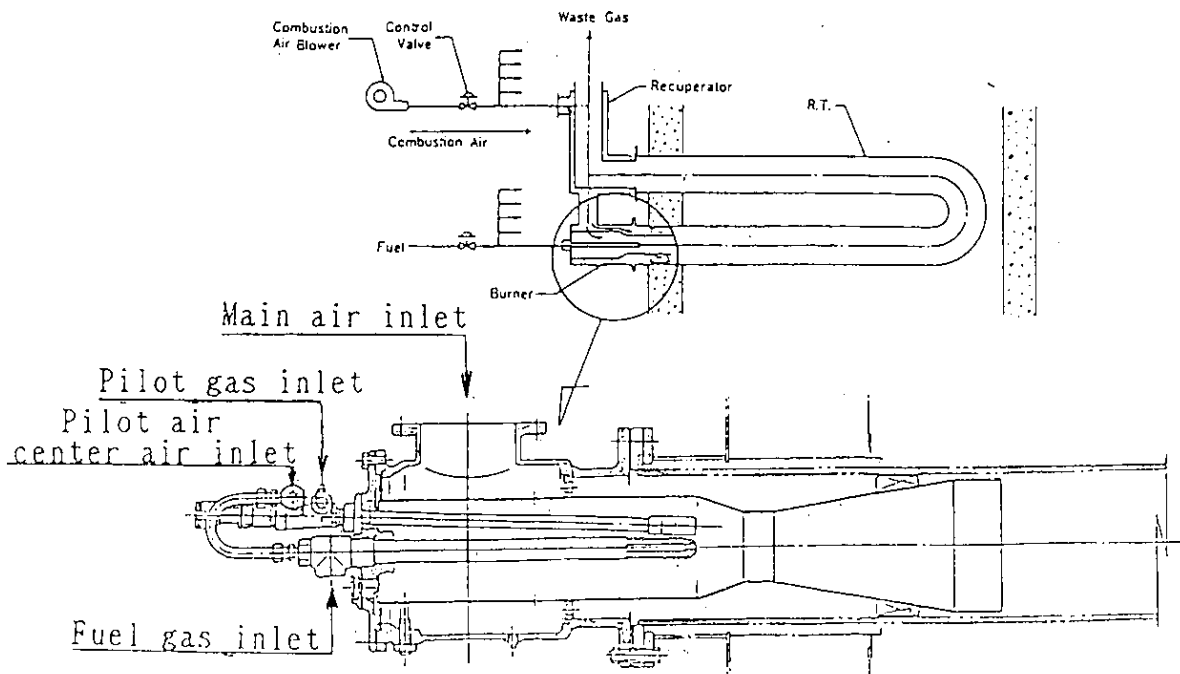


Radiative heating  
Flat flame gas burner (Model:HFB)

**Classification by Heating Method Indirect**

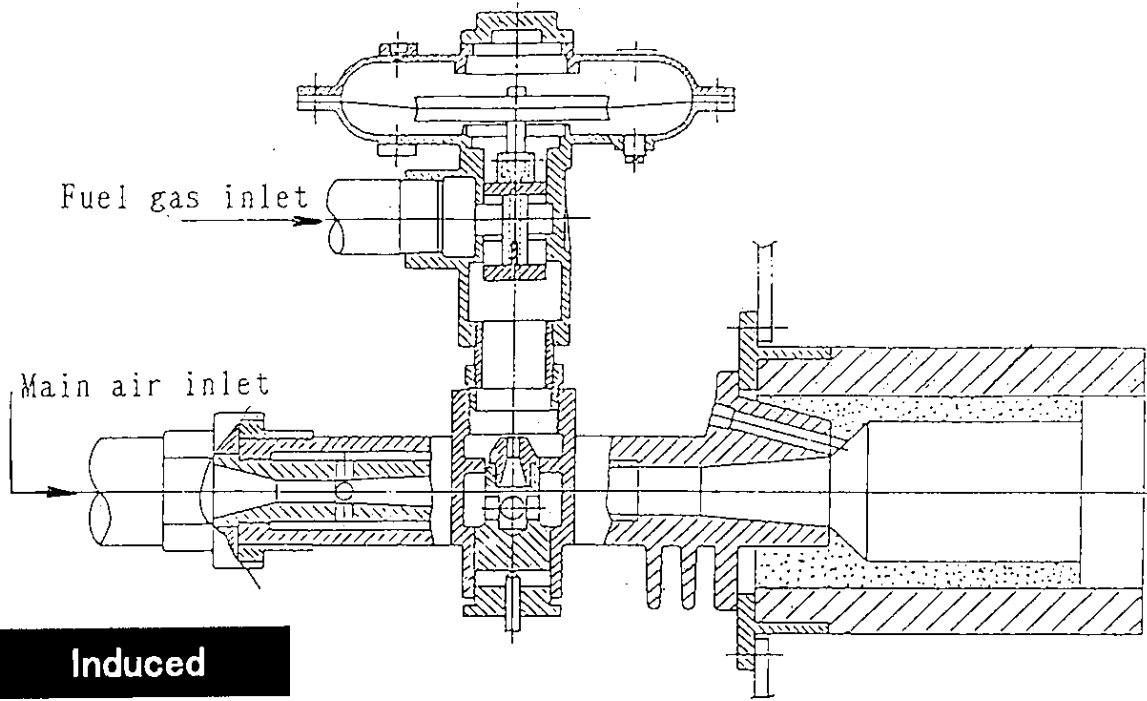


Single ended tube  
Concentric radiant tube unit (Model:CRB)



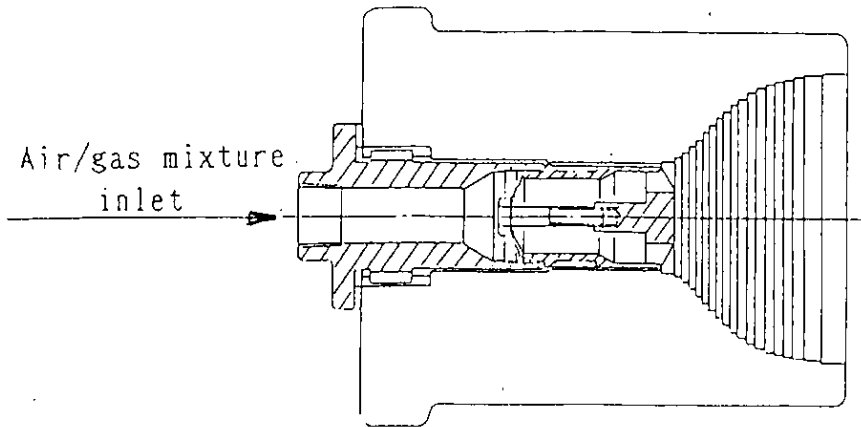
Both ended tube  
Low NOx radiant tube burner (Model:RBG-NR)

**Classification by Air/Fuel Mixing Method Premix**



**Induced**

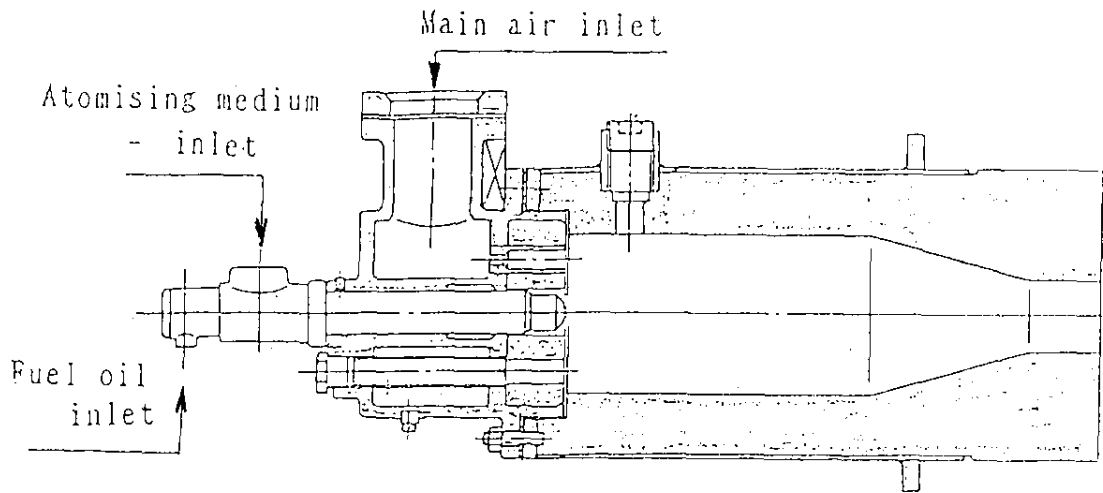
Low pressure velocity burner (Model:LP)



**Forced**

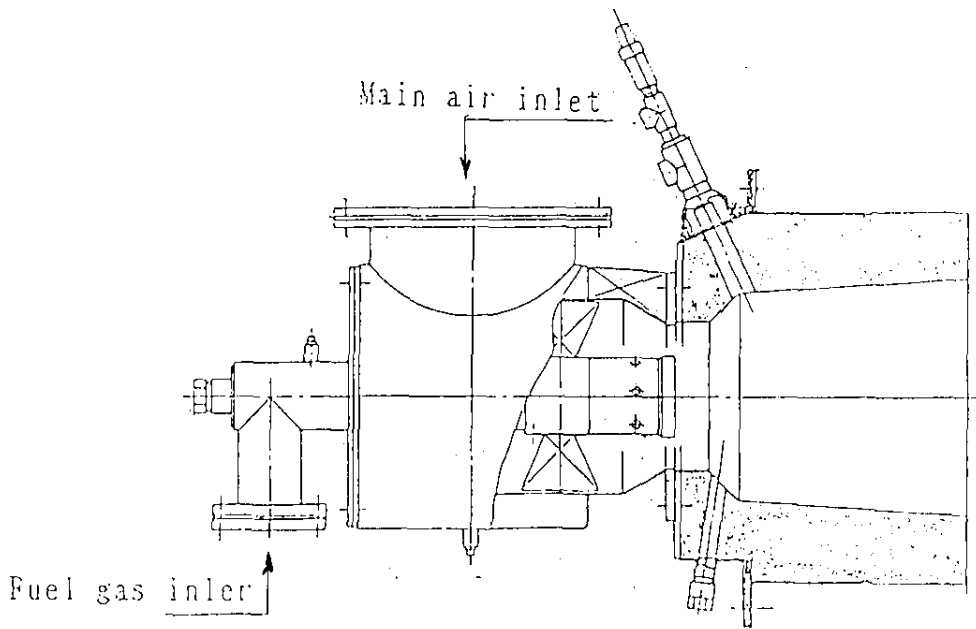
Radiation gas burner (Model:EFB)

**Classification by Air/Fuel Mixing Method Diffusion**



**Combustor**

High speed excess air burner (Model:HC)

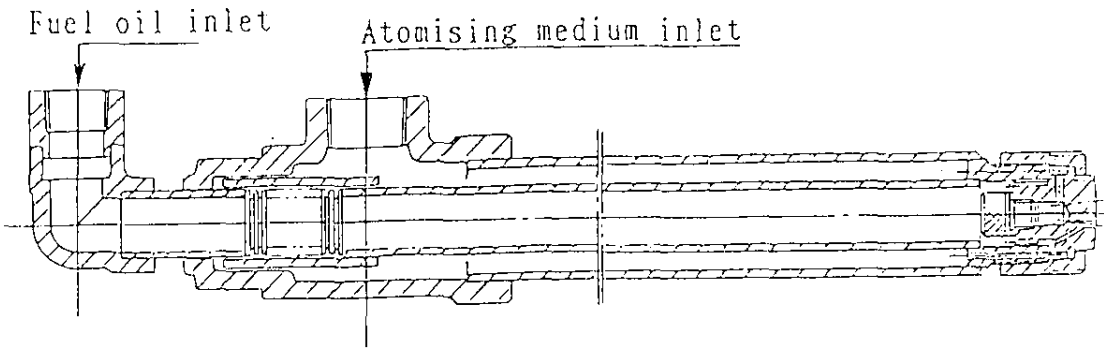


**Nozzle Mix**

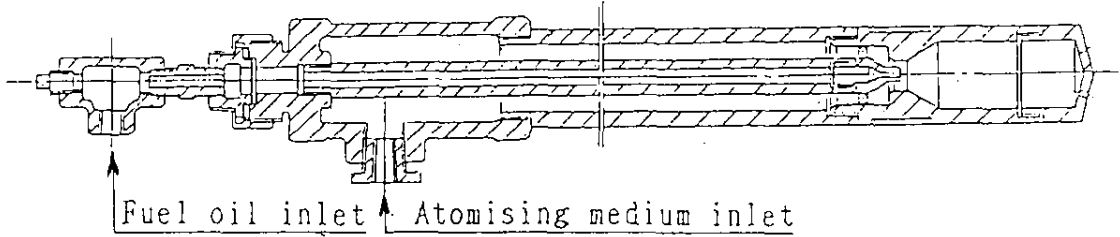
Nozzle mix gas burner (Model:NG)



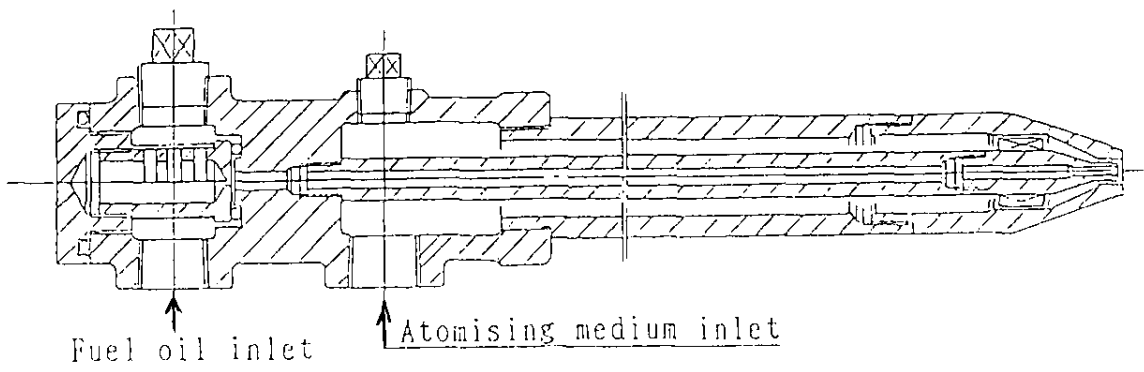
**Classification by atomizing Method Compressed Medium**



Y-jet atomiser (Model:SEA)

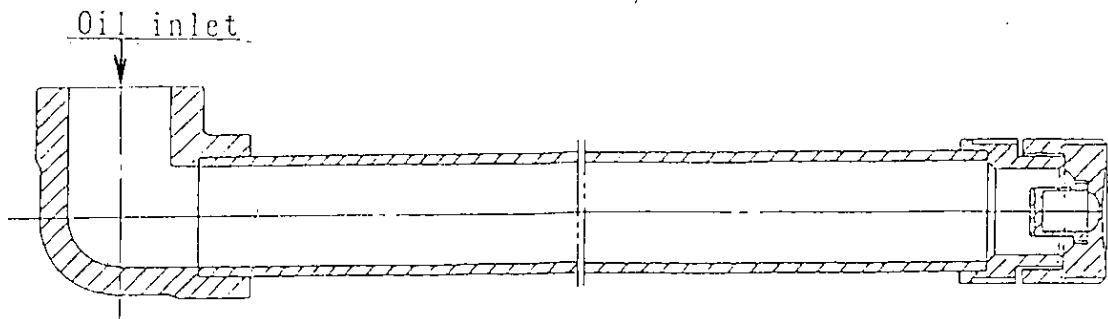


Internal mix atomiser (Model:MB)

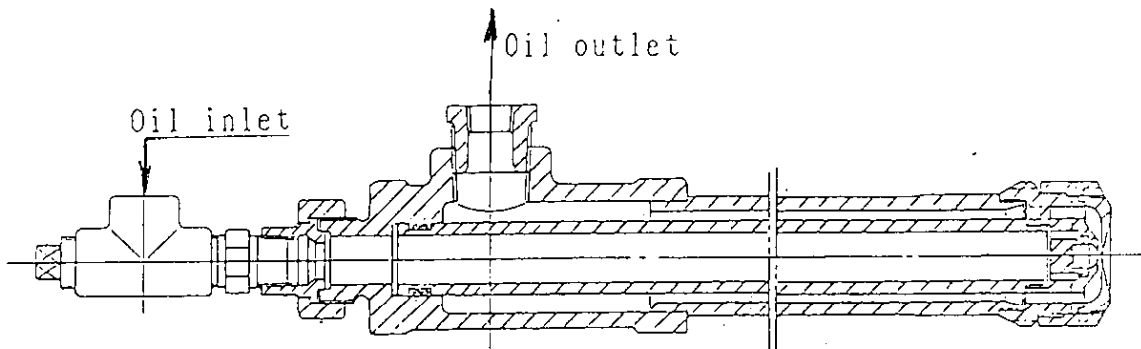


External mix atomiser (Model:HB)

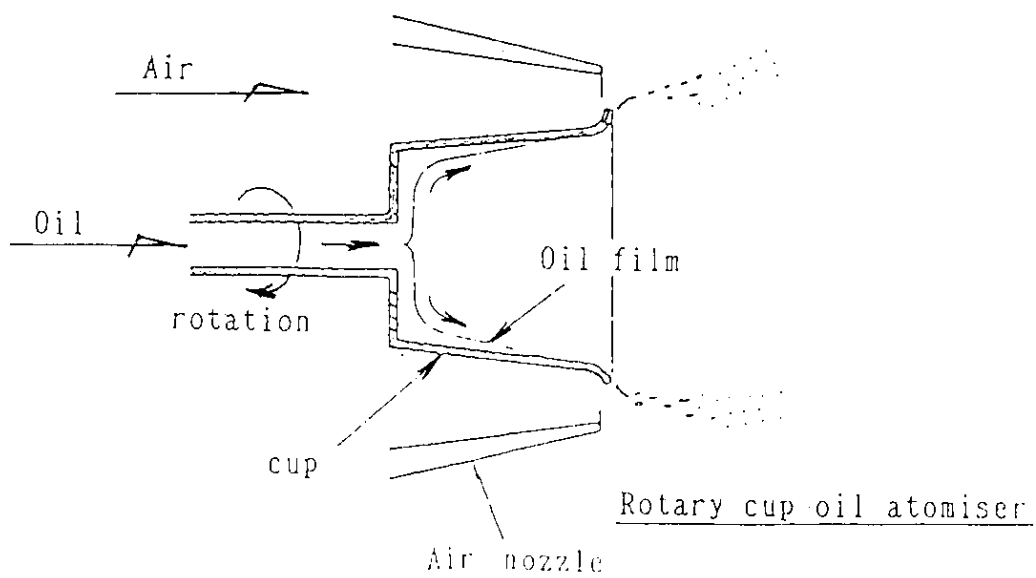
**Classification by atomizing Method No Atomizing Medium**



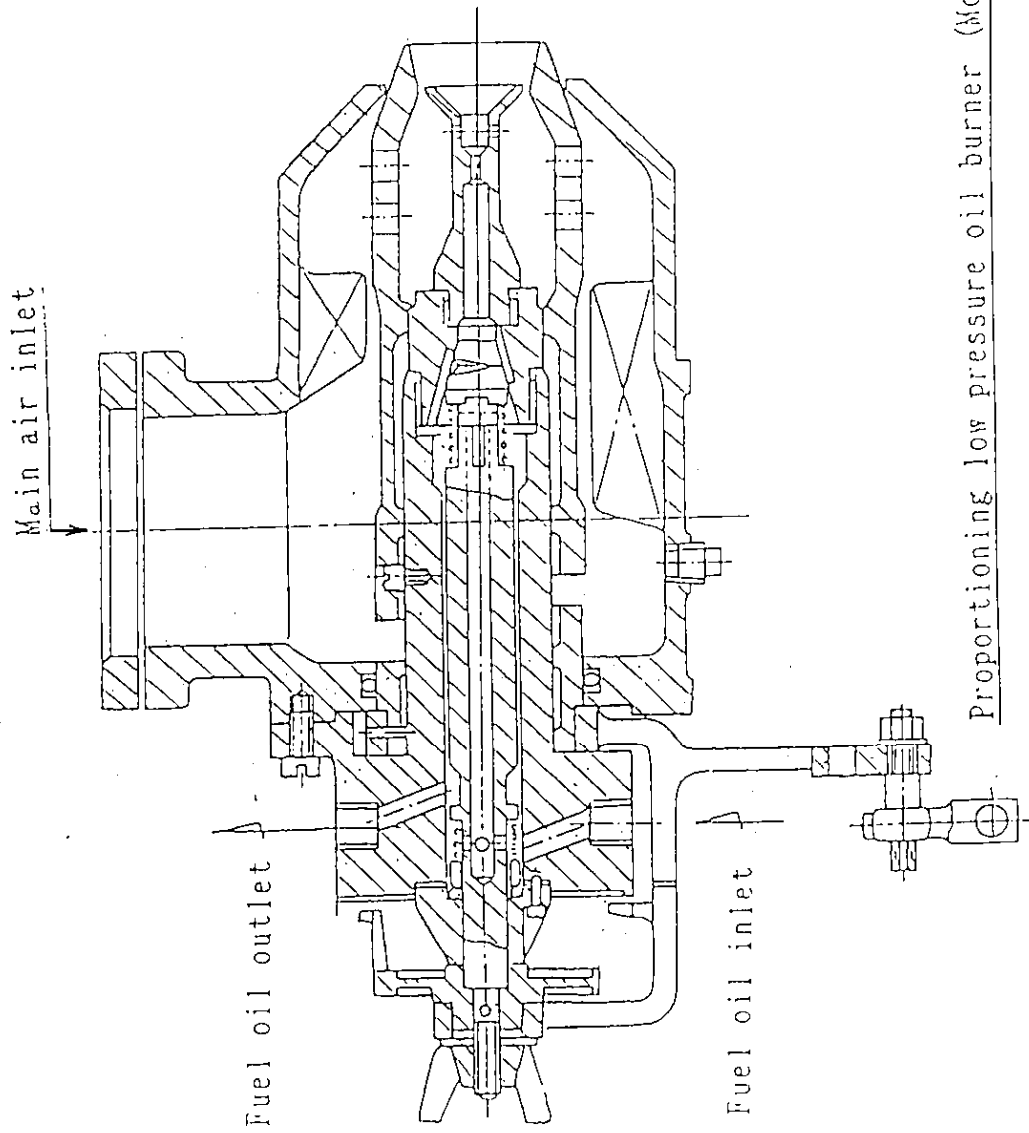
Pressure jet atomiser-No oil return



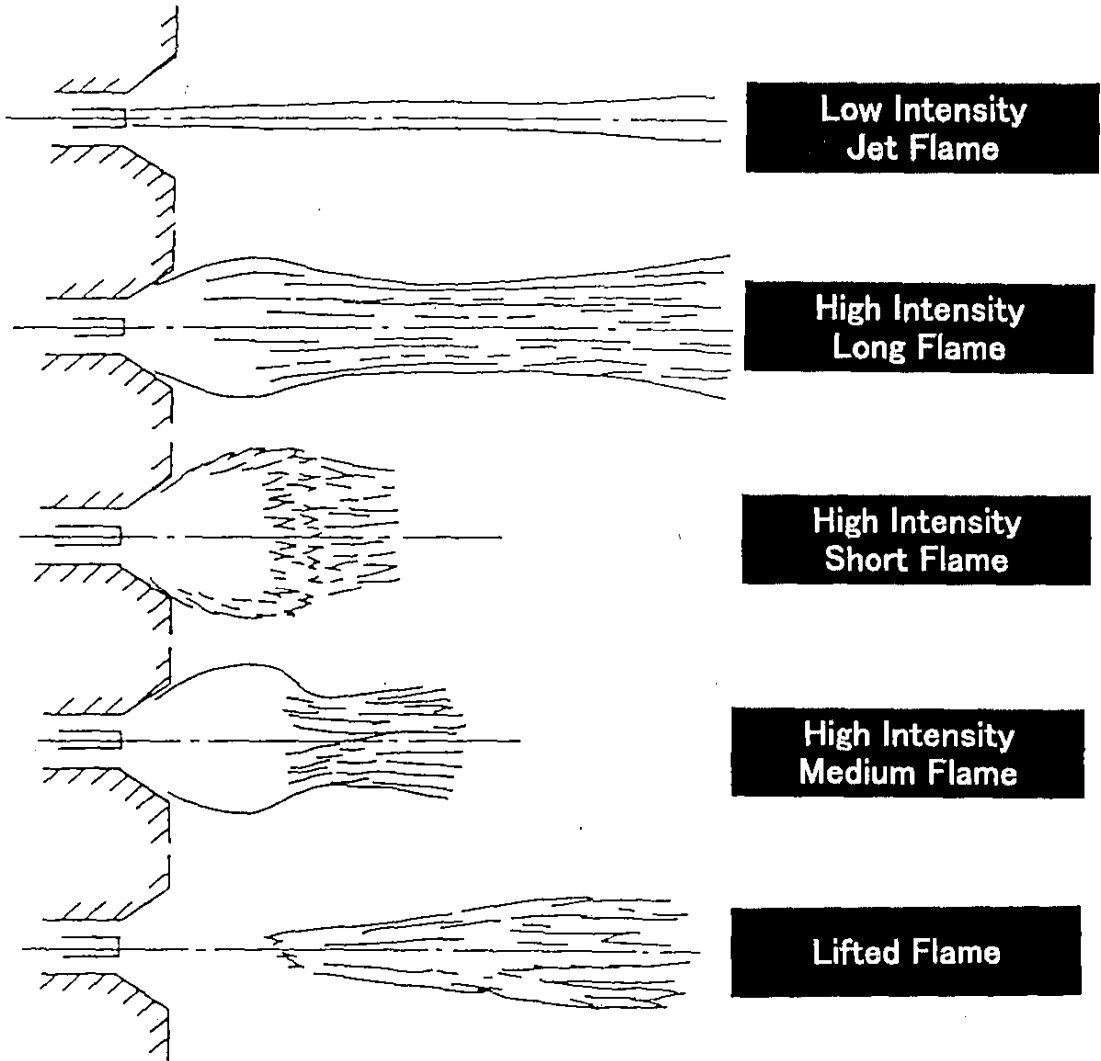
Pressure jet atomiser-oil return



**Classification by atomizing Method Low Pressure Air**



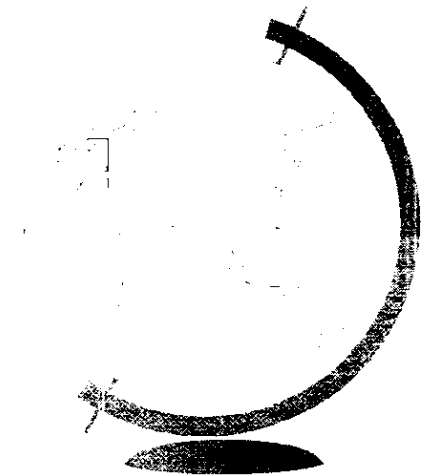
Proportioning low pressure oil burner (Model: PLB)



**Simple Flame Classification Scheme**

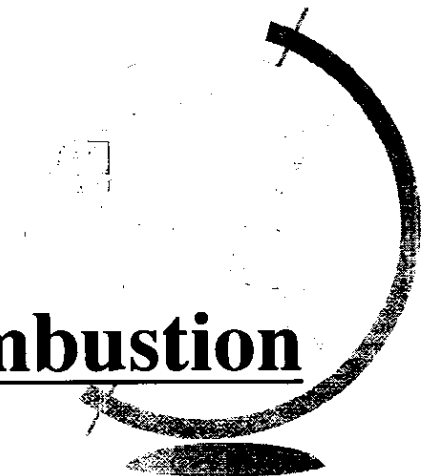
# New Combustion Technology

- ◆ Luminous Flame Gas Combustion
- ◆ **High Turn Down Combustion**
- ◆ Combustion of Low Calorific Value Fuel
- ◆ Pulse Combustion
- ◆ Reducing Combustion
- ◆ Fluidized Bed Combustion
- ◆ **Oxygen Enriched Combustion**



# New Combustion Technology

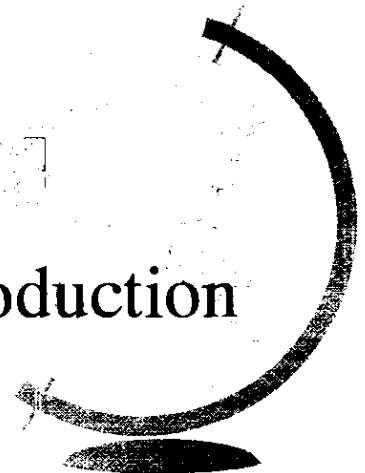
- ◆ Oxygen Deficient Combustion
- ◆ Coal Slurry
- ◆ Oil Residue
- ◆ Waste Products
- ◆ Blacking Technique
- ◆ Intelligent Burner System
- ◆ Regenerative Burner
- ◆ Computational Simulation of Combustion

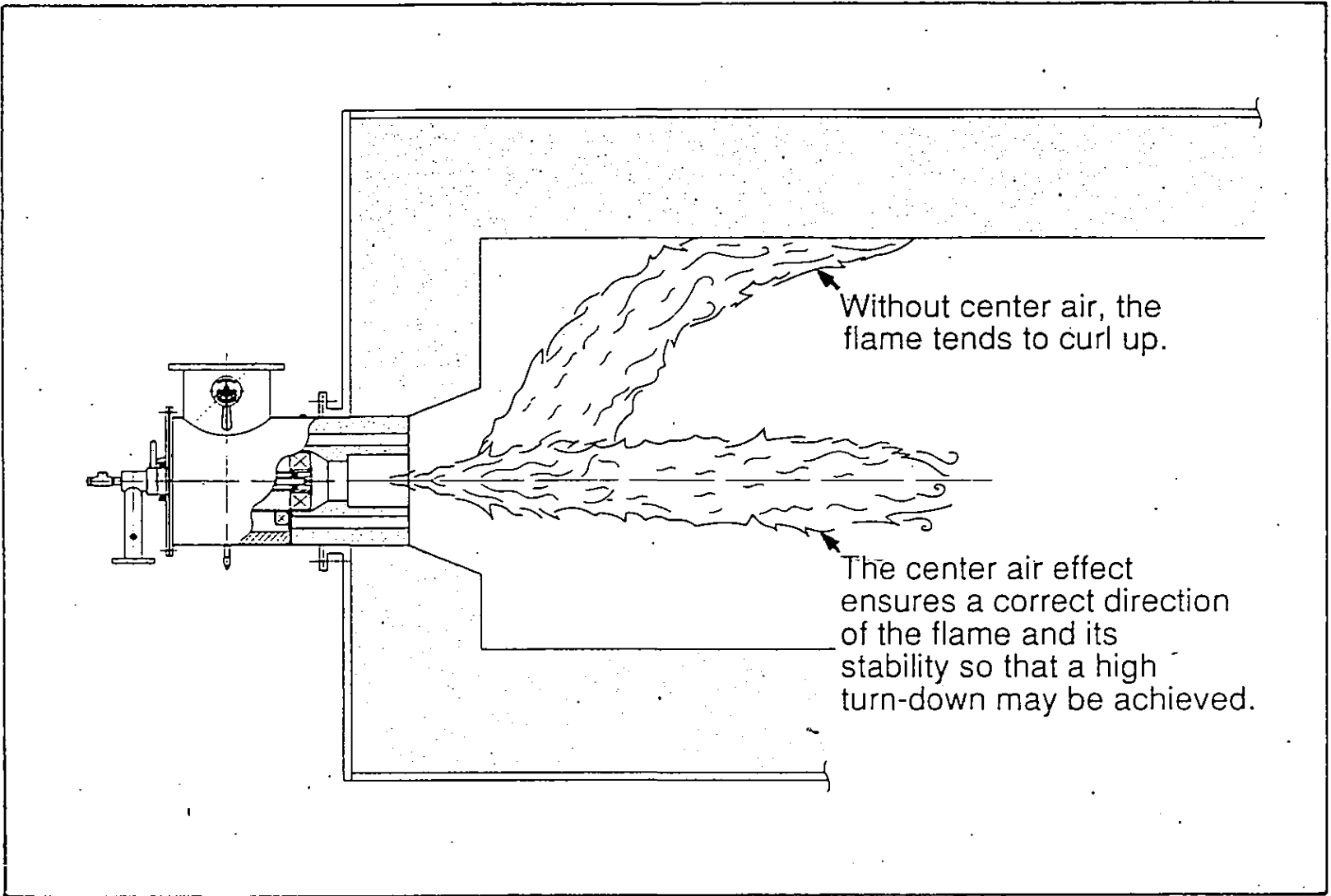


# New Combustion Technology (1)

## High Turn Down Combustion

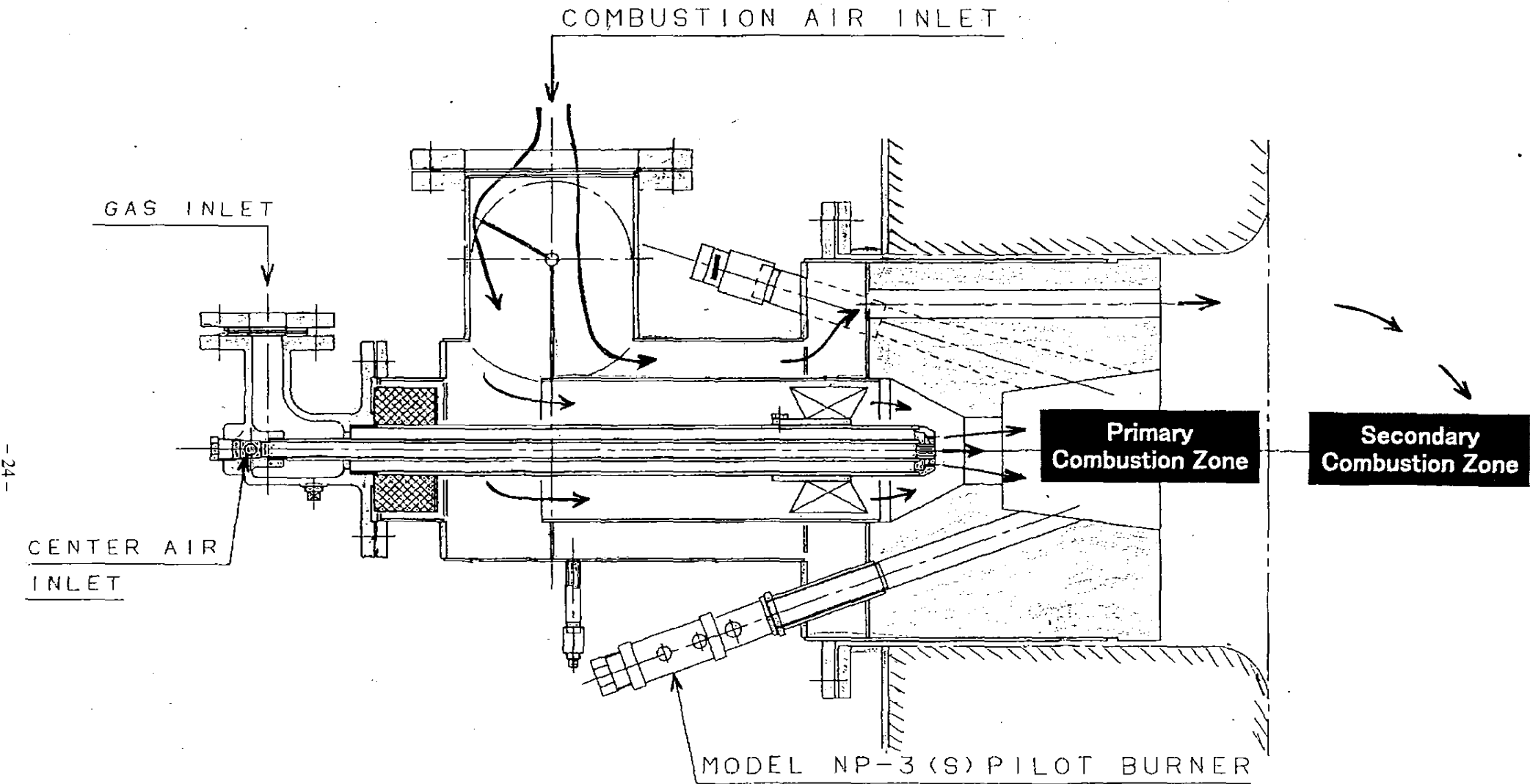
- ◆ T/D Ratio of Conventional Gas Burner ---- 1 : 5
- ◆ T/D Ratio of High Turn Down Burner ----- 1 : 10
- ◆ Type FHC Burner
  - High Turn Down Low NO<sub>x</sub> Burner
  - Center Air for improvement of Flame Direction
- ◆ Type DGB Burner
  - High Turn Down Burner ---- 1 : 20
  - Burner for Drying Oven in Automobile Production





**Center Air Effect**





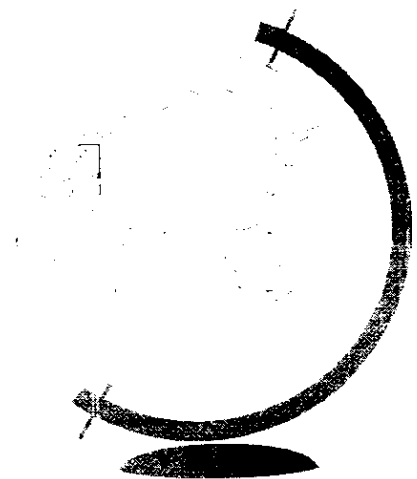
-24-

**Type FHC High Turn Down Low NOx Burner**

# New Combustion Technology (2)

## Oxygen Enriched Combustion

- ◆ Composition of Air :  $O_2 = 21 \text{ vol\%}$   $N_2 = .78 \text{ vol\%}$
- ◆ Advantages over Ambient Air
  - More elevated flame temp is achievable.
  - Air requirement in volume is less.
  - Flue gas volume is less.
- ◆ Disadvantage over Ambient Air
  - Short service life of refractory
  - Relatively High  $NO_x$  Emission

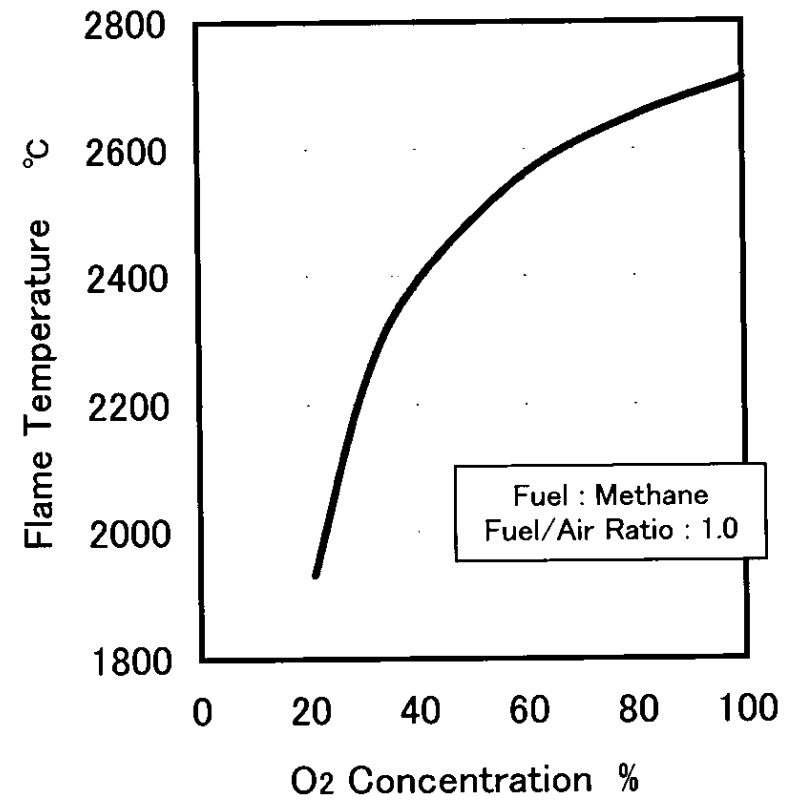
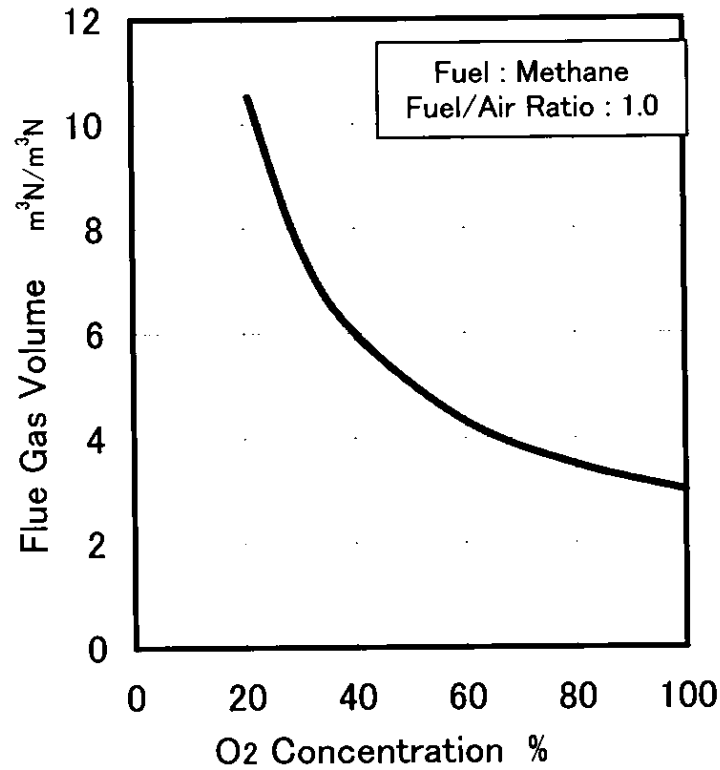


Composition	N <sub>2</sub>	O <sub>2</sub>	Ar	CO <sub>2</sub>	Ne	He	Total
Volume %	78.09	20.95	0.930	0.030	0.002	0.001	100.00
Weight %	75.52	23.15	1.280	0.046	0.001	0.000	100.00

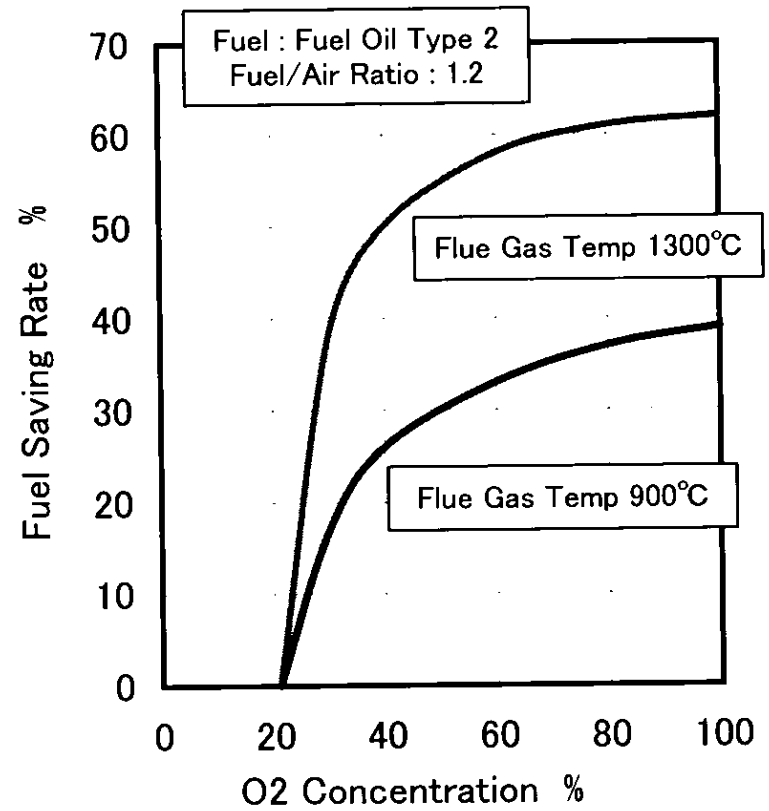
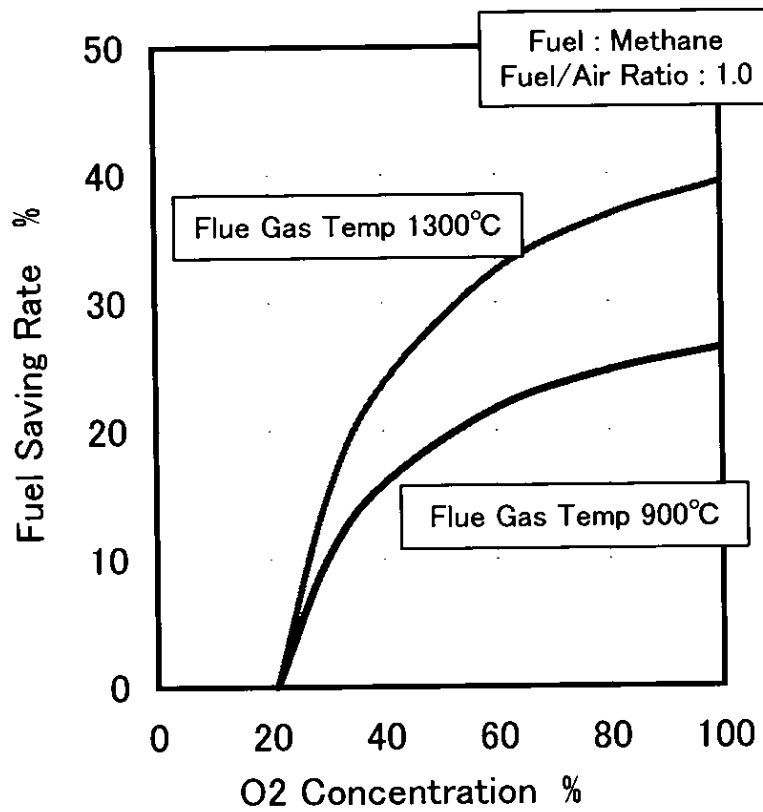
**Table 4. Composition of Air ( on Sea-level Ground )**

Oxygen Concentration in Comburent	Theoretical Comburent Volume	Theoretical Combustion Product m <sup>3</sup> N/m <sup>3</sup> N				Theoretical Flame Temperature
	m <sup>3</sup> N/m <sup>3</sup> N	CO <sub>2</sub>	H <sub>2</sub> O	N <sub>2</sub>	Total	°C
<b>100%</b>	<b>2.00</b>	<b>1.00</b>	<b>2.00</b>	<b>0.00</b>	<b>3.00</b>	<b>2711</b>
80%	2.50	1.00	2.00	0.50	3.50	2652
60%	3.33	1.00	2.00	1.33	4.33	2561
<b>50%</b>	<b>4.00</b>	<b>1.00</b>	<b>2.00</b>	<b>2.00</b>	<b>5.00</b>	<b>2492</b>
40%	5.00	1.00	2.00	3.00	6.00	2390
30%	6.67	1.00	2.00	4.67	7.67	2222
27%	7.41	1.00	2.00	5.41	8.41	2147
25%	8.00	1.00	2.00	6.00	9.00	2087
23%	8.70	1.00	2.00	6.70	9.70	2016
<b>21%</b>	<b>9.52</b>	<b>1.00</b>	<b>2.00</b>	<b>7.52</b>	<b>10.52</b>	<b>1932</b>
18%	11.11	1.00	2.00	9.11	12.11	1775
12%	16.67	1.00	2.00	14.67	17.67	1335

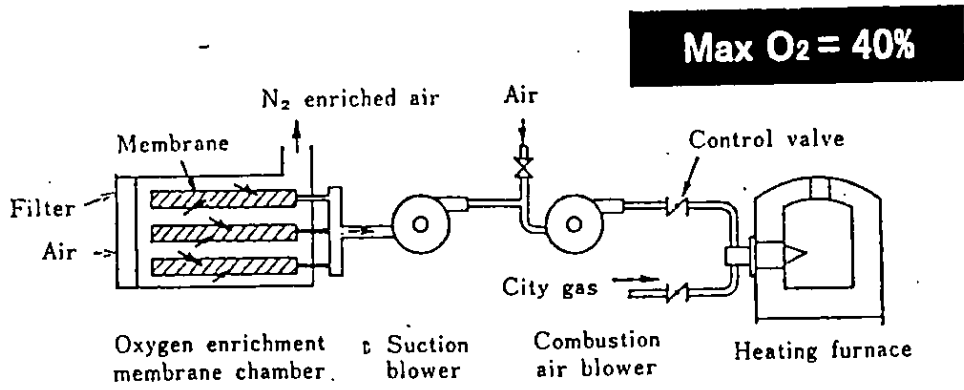
Table 5. Theoretical Combustion Characteristics of Methane in case of Changes in Oxygen Concentration



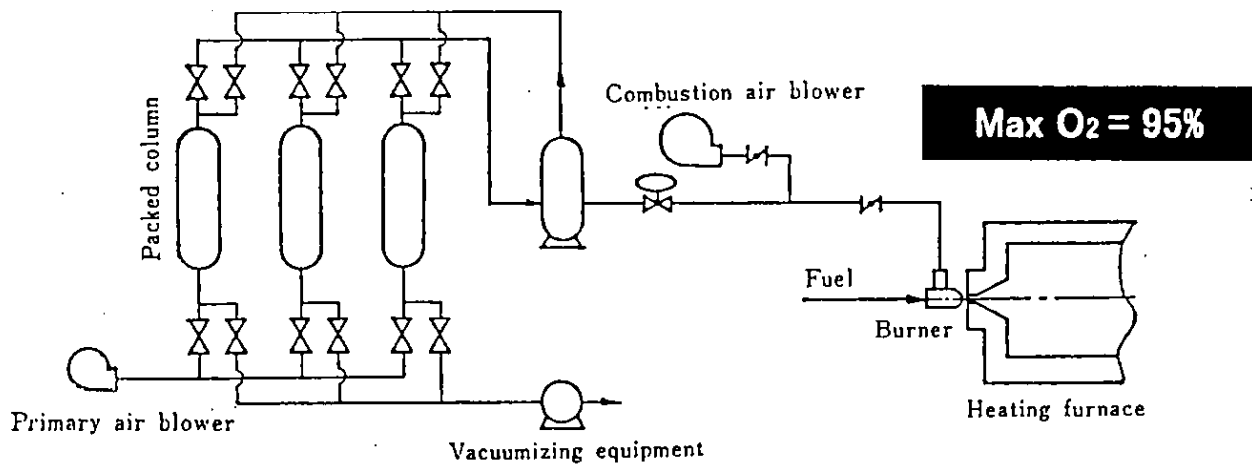
Theoretical Combustion Characteristics of Methane  
in case of Changes in Oxygen Concentration



Fuel Saving Rate of Methane & Fuel Oil Type2  
in case of Changes in Oxygen Concentration



**Membrane Method Oxygen Generator**



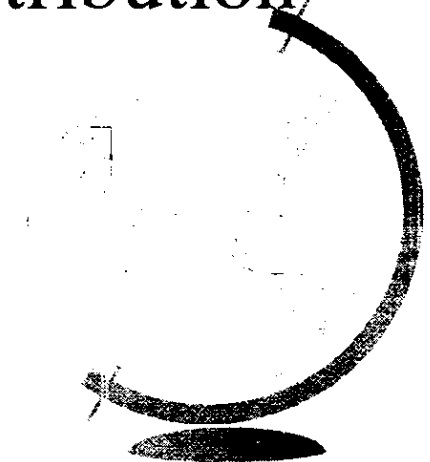
**Pressure Swing Adsorption (PSA) Oxygen Generator**

# New Combustion Technology (3)

## Regenerative Burner

### ◆ Advantages

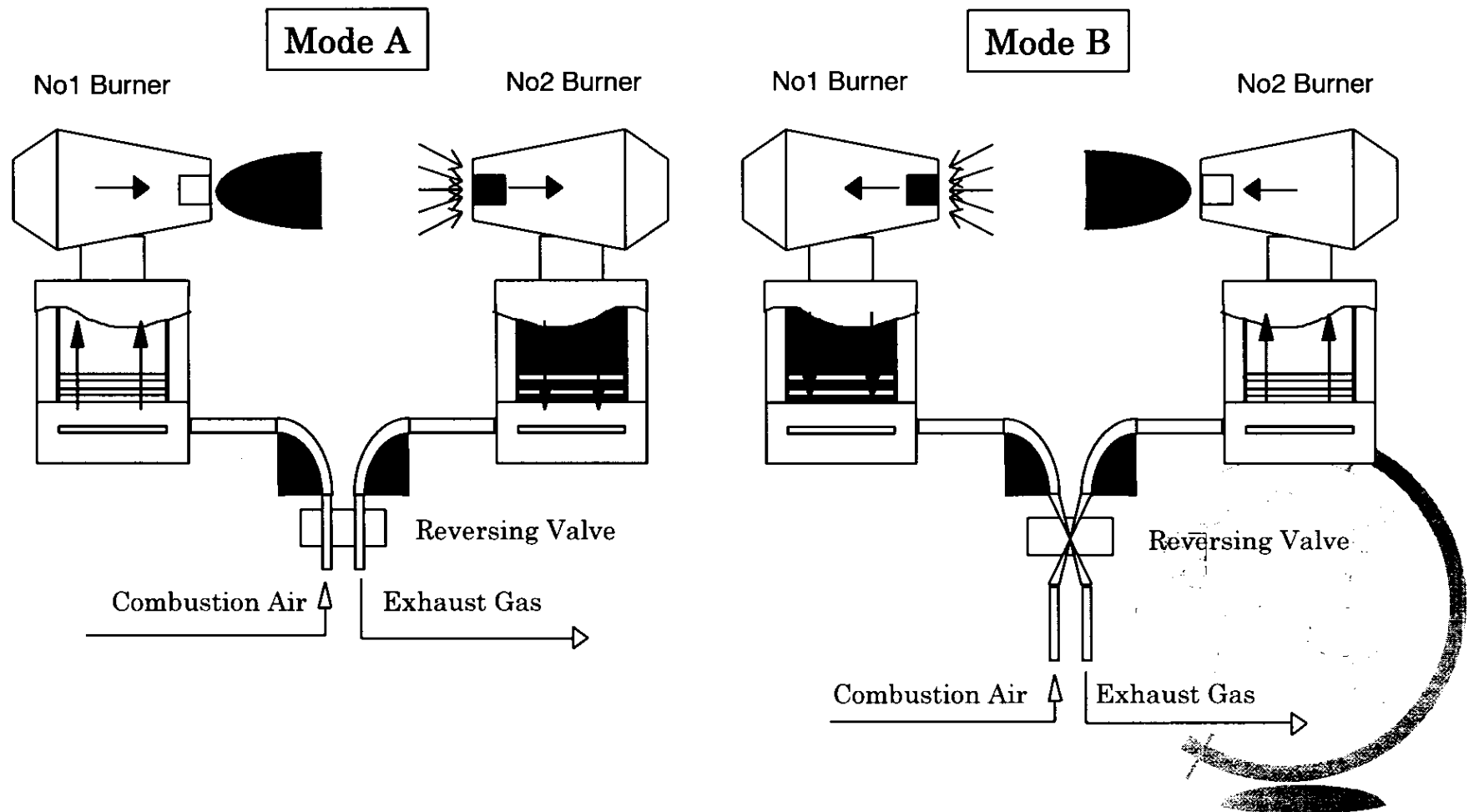
- Waste Gas Heat Recovery Max 90%
- Waste Gas Temp. : 1200°C
- Max. Preheated Air Temp. : 1080°C
- Pulse Firing for Uniform Temp. Distribution
- Heat Exchange in the Burners
- Shorter Furnace Length





# New Combustion Technology (3)

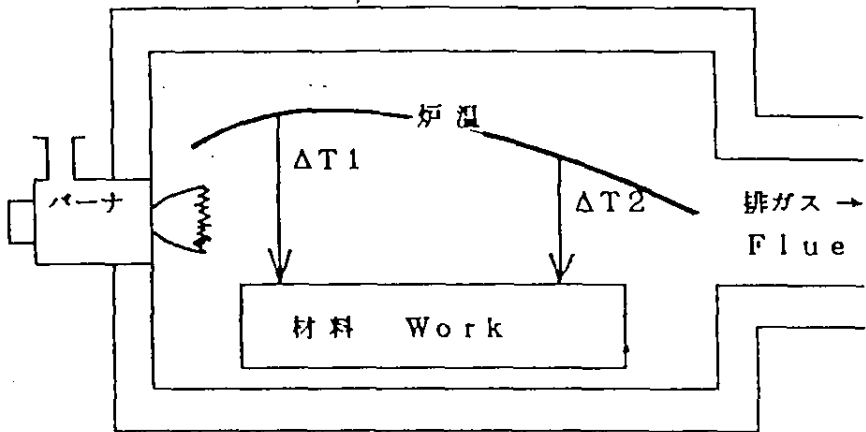
## Control Logic of Regenerative Burner



従来の燃焼炉

Conventional

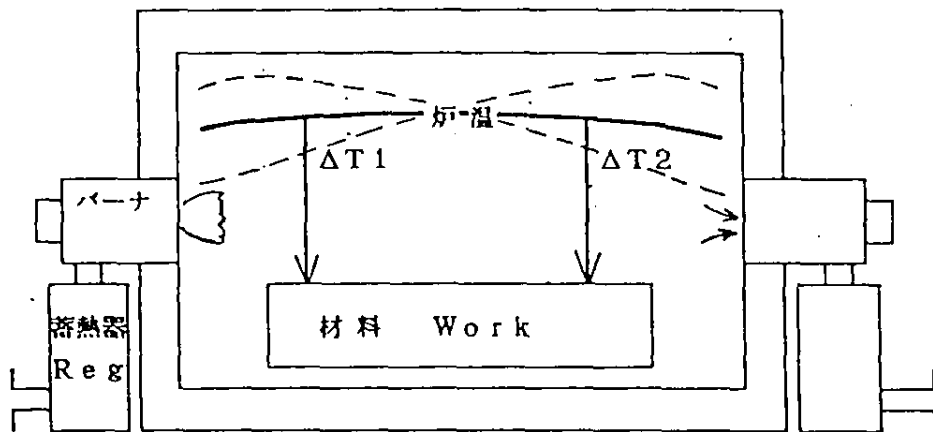
$\Delta T1 > \Delta T2$



蓄熱式バーナを使用する燃焼炉

Regenerative Furnace

$\Delta T1 = \Delta T2$



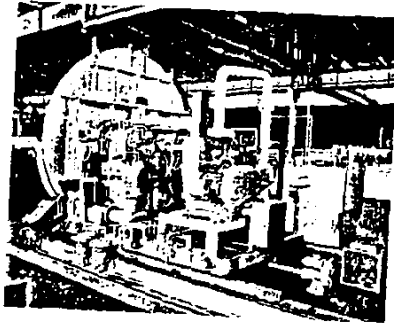
蓄熱式バーナの温度分布

Temp. Distribution by Regen. Burner

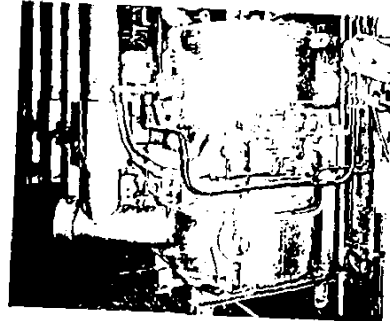
**Chugai Ro**

# New Combustion Technology (3)

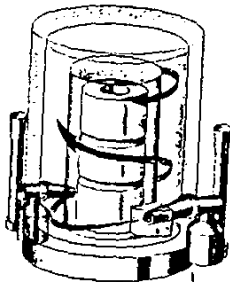
## Application Examples of Regenerative Burner



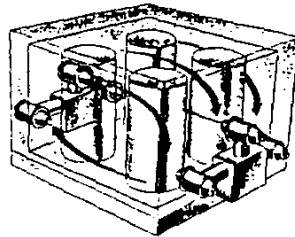
RCB regenerative burners fitted to a ladle preheater



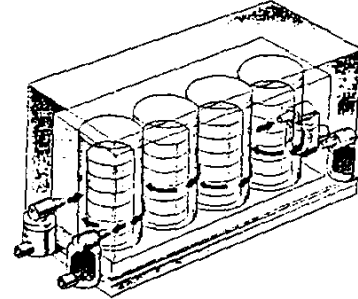
RCB regenerative burners fitted to a steel reheating furnace



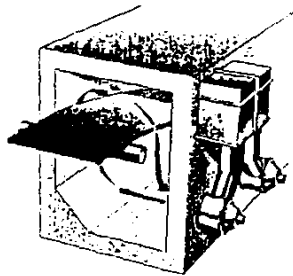
Bell type coil annealing furnace



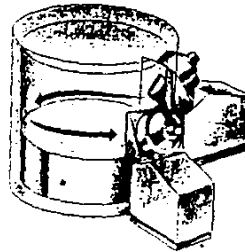
Cross fired coil annealing furnace



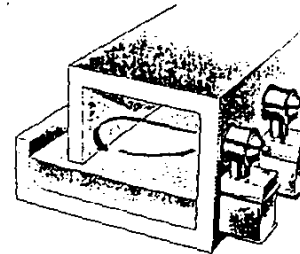
Corner fired coil annealing furnace



Catenary type continuous steel strip heat treating furnace



Round reverberatory aluminum melting furnace



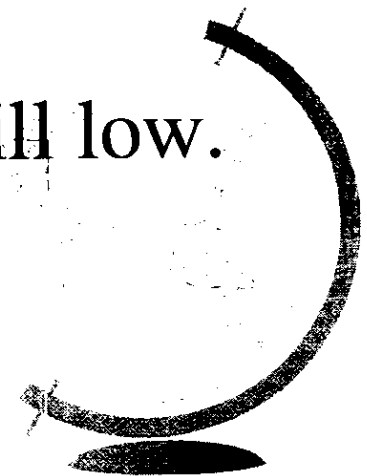
Front well type reverberatory aluminum melting furnace



# New Combustion Technology (4)

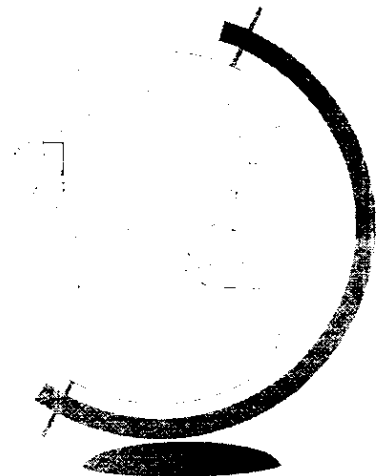
## Computational Simulation of Combustion

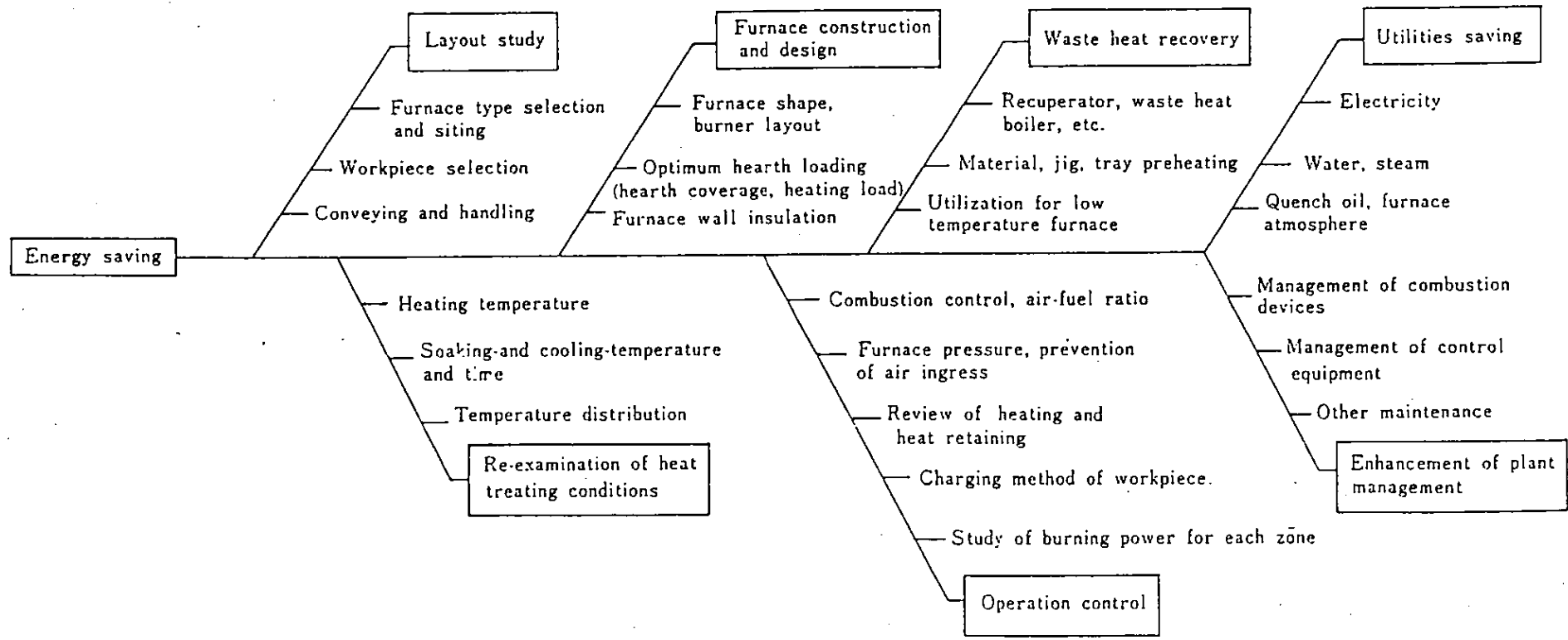
- ◆ Analysis Cords
  - Fluent, Star-CD, etc...
- ◆ Simulated Results
  - Distributions of Fluid Temperature, Fluid Flow and Gas Species.
- ◆ At present, accuracy of the results is still low. However, in the near future, it will be improved.



# Combustion Technology for Energy Saving

- ◆ Layout study
- ◆ Re-examination of Heat Treating Condition
- ◆ Furnace Construction and Design
- ◆ Operation Control
- ◆ Waste Heat Recovery
- ◆ Utilities Saving
- ◆ Enhancement of Plant Management





**Factor of Energy Saving Measures**

# Combustion Technology for Energy Saving

## --- Excess Air Control ---

### ◆ Definition of Excess Air Ratio

Actual Combustion Air Flows (m<sup>3</sup>N/kg-fuel)

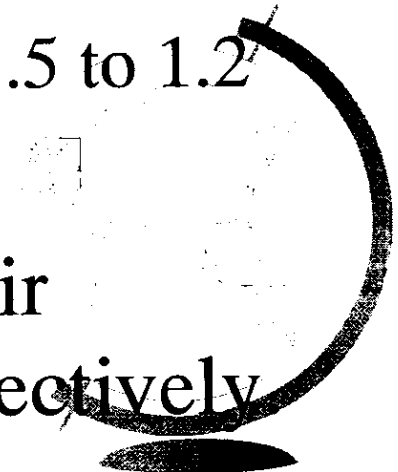
Theoretical Air Requirement (m<sup>3</sup>N/kg-fuel)

ex) ▪ Flue Gas Temp. = 1300°C

▪ Excess Air Ratio Change from 1.5 to 1.2

▪ Fuel Saving Rate = 40.2%

### ◆ Combined with preheat and excess air technology control is much more effectively



Furnace Temperature °C	Air Ratio Before Correction	Air Ratio After Correction				
		1.40	1.30	1.20	1.10	1.00
700	1.50	3.9	7.4	10.7	13.8	16.7
	1.40		3.8	7.3	10.5	13.5
	1.30			3.7	7.0	10.1
	1.20				3.5	6.7
	1.10					3.4
900	1.50	6.2	11.7	16.6	21.0	25.0
	1.40		5.9	11.3	16.0	20.2
	1.30			5.7	10.7	15.2
	1.20				5.3	10.1
	1.10					5.1
1100	1.50	10.3	18.6	25.6	31.4	36.4
	1.40		9.4	17.3	23.8	29.4
	1.30			8.7	15.9	22.1
	1.20				7.9	14.7
	1.10					7.4
1300	1.50	18.3	31.0	40.2	47.3	52.9
	1.40		15.7	27.2	35.9	42.7
	1.30			13.7	23.9	32.1
	1.20				11.9	21.3
	1.10					10.7

Table 6. Fuel Saving Rate (%) on Excess Air Control  
(Fuel Oil Type 1)



# Combustion Technology for Energy Saving

## --- Heat Recovery from Flue Gas ---

### ◆ Outline of Air Preheater

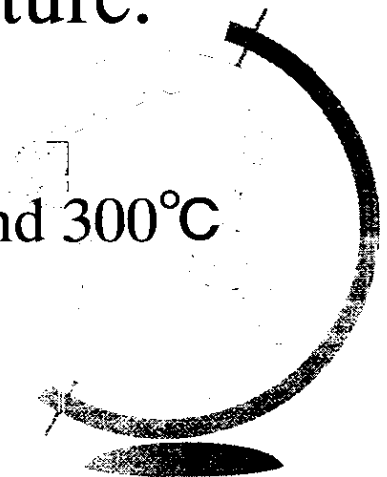
- Recuperator and Regenerator

### ◆ Fuel saving rate depends on preheated air temperature and exhaust gas temperature.

ex) ▪ Kerosene, Excess Air Ratio=1.2

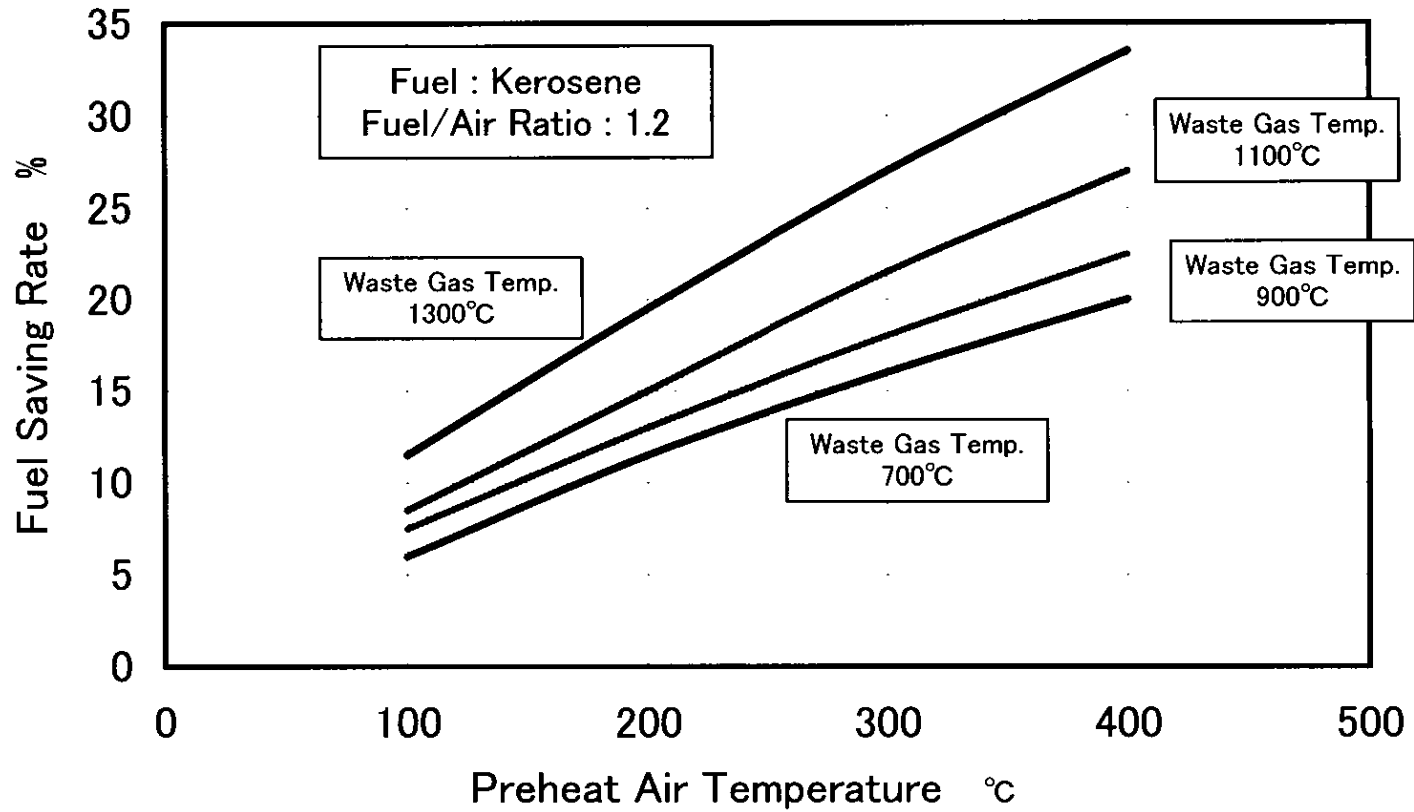
- Flue Gas and Preheated Air Temp. = 900 and 300°C

- Fuel Saving Rate = 18.4%

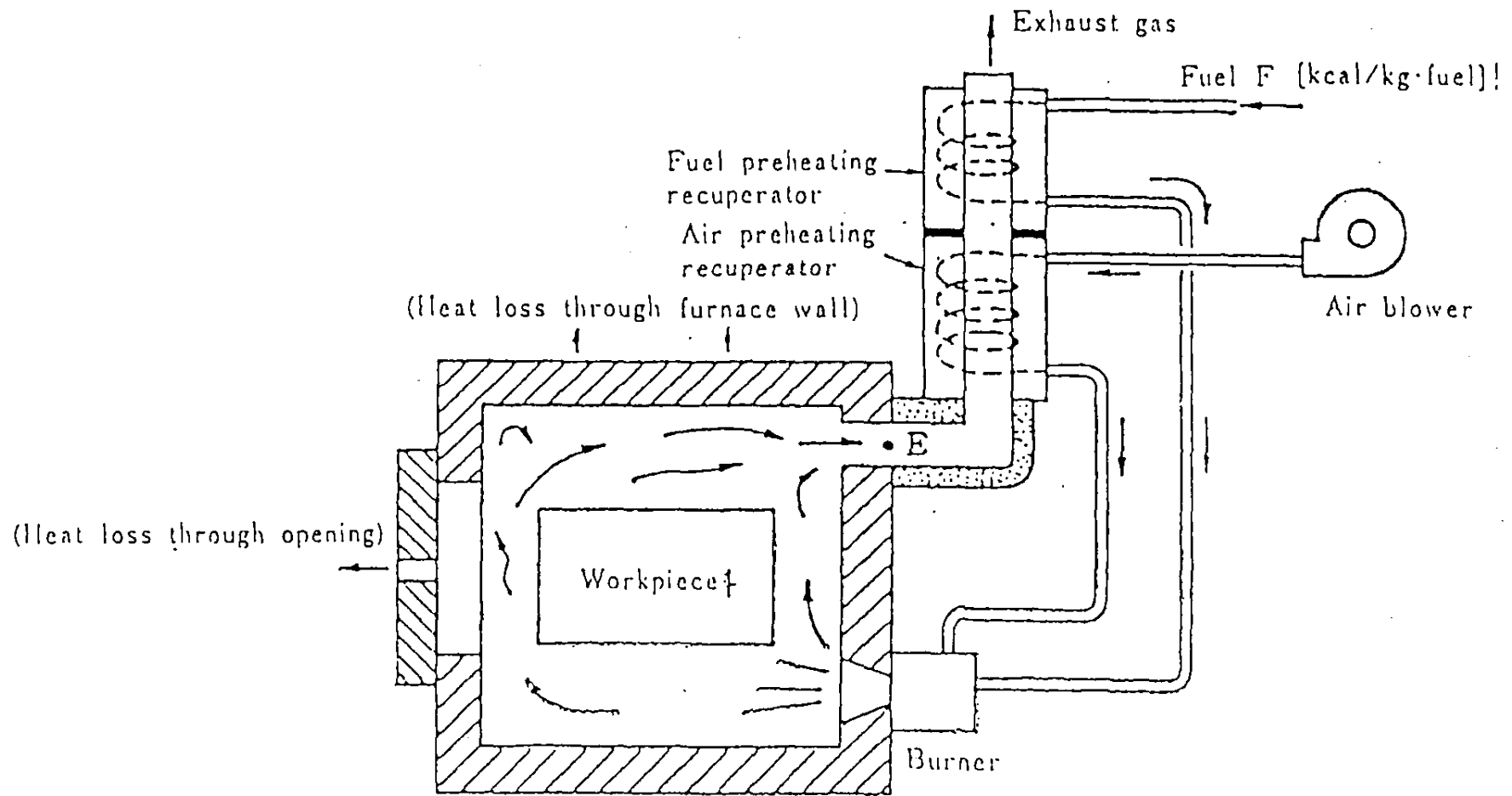


Type				Exhaust Gas Temp. Limit	Preheated Air Temp.	Applied Furnace
Recuperator	Metallic	Flue Type	Convection type Multi-tube Type	1000°C Max	300~600°C	Reheating Furnace Heat Treating Furnace Other Industrial Furnace
		Chimney Type	Radiation Type Radiation+Convection Type	1000~1300°C		
	Ceramic (Tile)		Armco Type Stein Type	1200~1400°C	400~700°C	Soaking Furnace Glass Oven
Regenerator	Conventional Type			1000~1600°C	600~1300°C	Coke Oven Hot Blast Furnace Glass Oven (Melter)
	Rotary Regenerating Type			600°C Max	100~300°C	Boiler Hot Blast Furnace Oil Refinery Furnace
	Regenerative Burner Type			1000~1300°C	900~1200°C	Reheating Furnace Heat Treating Furnace Other Industrial Furnace

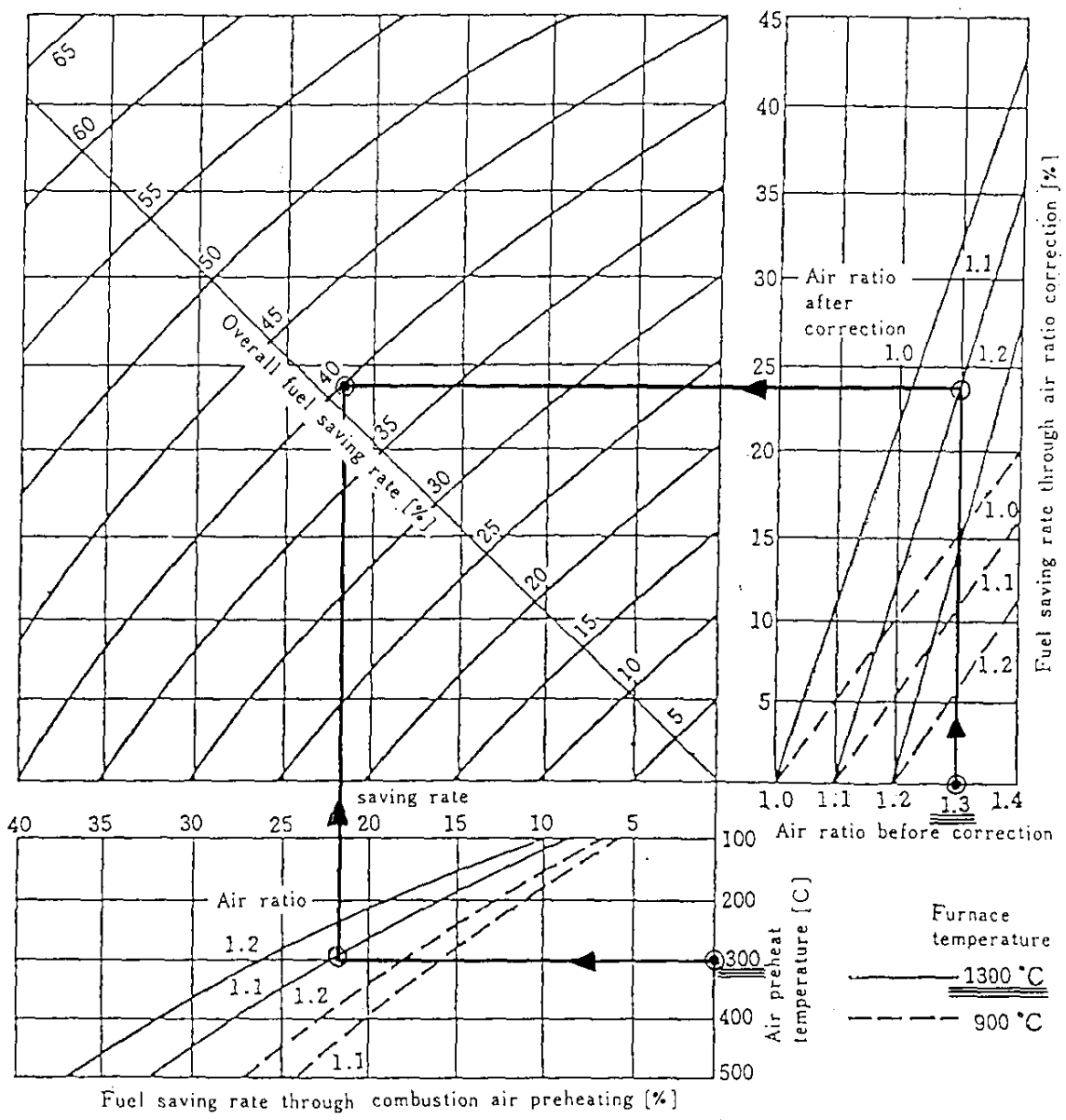
Table 7. Outline of Air Preheater



**Fuel Saving Rate through Air Preheating**



**Basic Conceptual Diagram of Waste Heat Utilization**

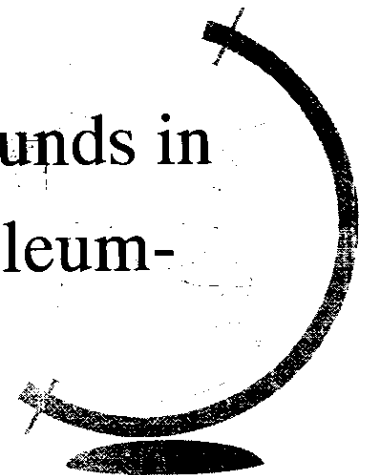


**Overall Fuel Saving Rate through Combustion Air Preheating and Air Ratio Correction (Fuel Oil Type 2)**

# Combustion Technology for Low Environmental Pollution

## ◆ Classification of NO<sub>x</sub>

- Thermal NO<sub>x</sub> is generated when atmospheric N<sub>2</sub> is heated to high temperatures. Their generation mechanisms include Zeldovich
- Prompt NO mechanism is specific to the combustion of hydrocarbon fuels.
- Fuel NO<sub>x</sub> is generated from nitrogen compounds in fuel, such as quinoline and pyridine in petroleum-based fuels and coal.



# Combustion Technology for Low Environmental Pollution

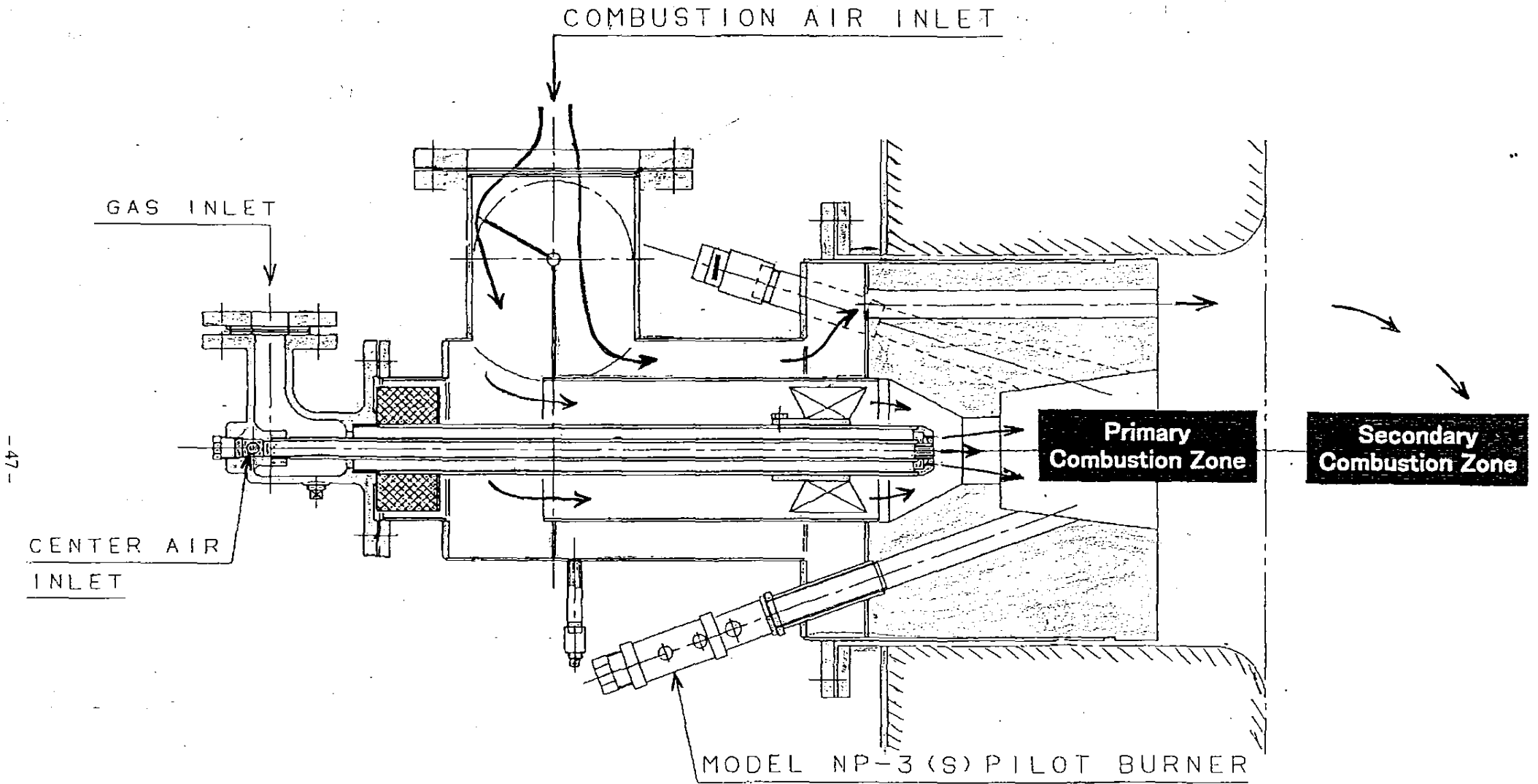
## ◆ Impact of NO<sub>x</sub>

NO<sub>2</sub> turn into photochemical oxidants, thereby giving rise to photochemical smog.

## ◆ NO<sub>x</sub> reduction measures

- Combustion control
- Use of low NO<sub>x</sub> burners
- Modification of combustion process
- Denitrification equipment

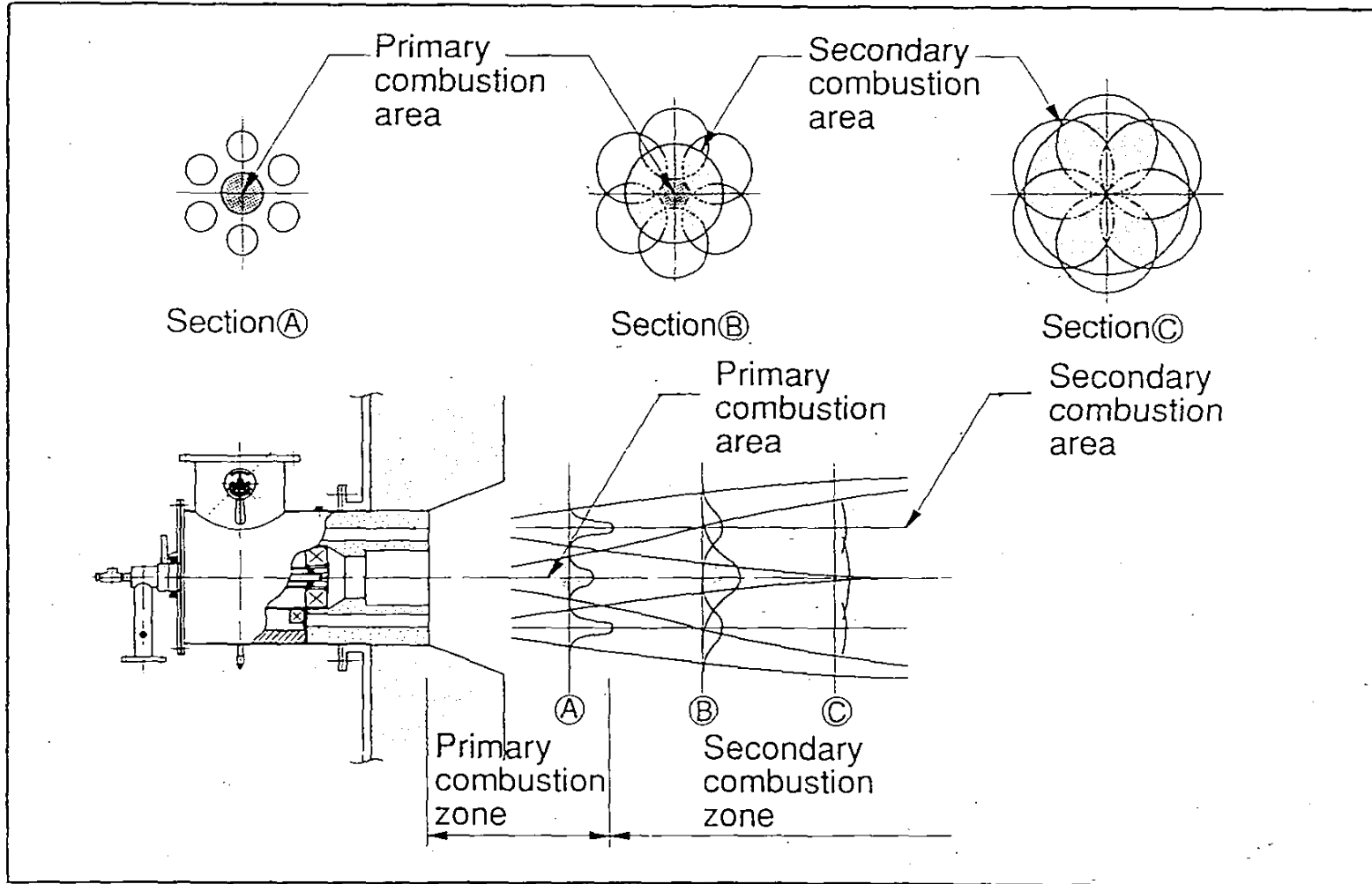




-47-

**Type FHC High Turn Down Low NOx Burner**





**NOx Reduction Method on FHC Burner**

No.	Operation parameter	Chart of NOx variation pattern	Remarks
1	Burner air ratio		Burner air ratio: when large, NOx → large (O <sub>2</sub> partial pressure of flame → large) If it further increases, NOx → small (Fall in flame temperature)
2	Preheated air temperature		Preheated air temperature: when large, NOx → large (Rise in flame temperature)
3	Furnace temperature		Furnace temperature: when large, NOx → large (Rise in flame temperature)
4	Furnace liberation rate (Furnace cross section liberation rate or furnace volume liberation rate)		Furnace liberation rate: when large, NOx → large (Rise in flame temperature due to small heat dissipation into surroundings)
5	Fuel type		Fuel with large theoretical combustion temperature → more NOx
6	Fuel N content ratio		Fuel N content ratio: large → more NOx
7	Burner combustion capacity		Burner combustion capacity: large → more NOx (Small heat dissipation into surroundings → Rise in flame temperature)

**Relationship between Burner Operation Parameters and Amount of NOx Generated (1)**

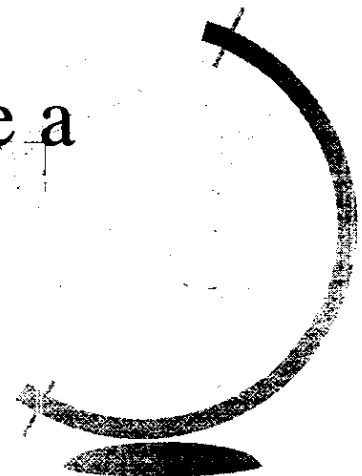
No.	Operation parameter	Chart of NOx variation pattern	Remarks
8	Burner register pressure differential		Burner register pressure differential: large → more NOx (Short flame due to better mixing → rise in flame temperature)
9	Furnace air ratio		Furnace air ratio: large → more NOx (when there is a supply of O <sub>2</sub> from sources other than the burner, such as intruding air) (O <sub>2</sub> partial pressure of flame → large)
10	Furnace pressure		Furnace pressure: large → more NOx
11	Steam consumption (steam spray or suction)		Steam consumption: large → less NOx (Fall in flame temperature)
12	Amount of flue gas recirculation		Amount of flue gas recirculation: large → less NOx (Decreased O <sub>2</sub> partial pressure of flame → fall in flame temperature)

**Relationship between Burner Operation Parameters and Amount of NOx Generated (2)**

# Combustion Technology for Low Environmental Pollution

## ◆ Impact of Sox

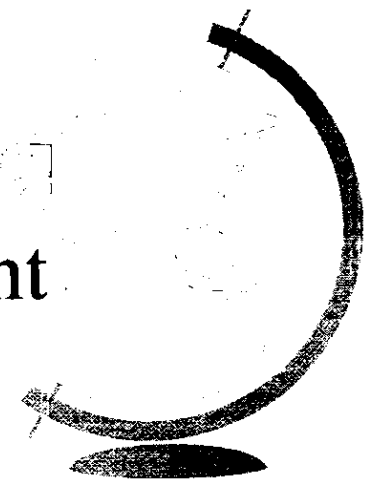
- (1)  $\text{SO}_2$  released into the atmosphere causes acid rain and exerts an enormous impact on ecosystems.
- (2) Condensed sulfuric acid can corrode a combustion facility.



# Combustion Technology for Low Environmental Pollution

## ◆ SO<sub>x</sub> reduction measures

- All combustible sulfur contained in a fuel turns into SO<sub>x</sub>.
- It is impossible to reduce SO<sub>x</sub> via combustion technology.
- Switch to Low-sulfur Fuels
- Flue Gas Desulfurization Equipment



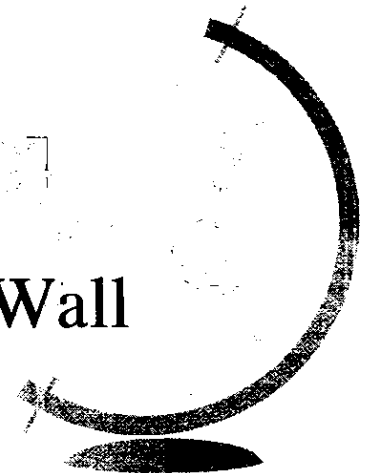
# Industrial Furnace Conservation Techniques

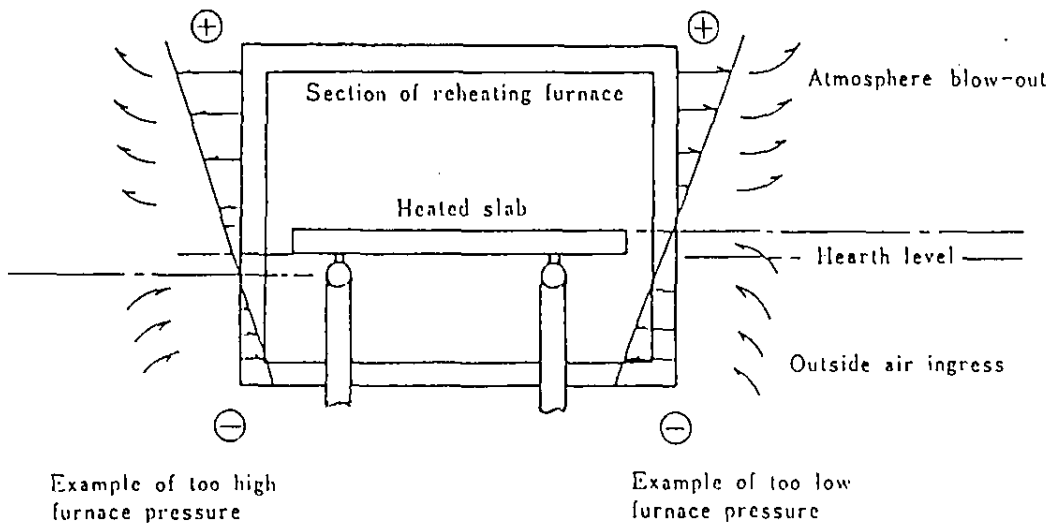
## ◆ Furnace Pressure Control

- Negative : Adversely Affect to Products Quality and Thermal Efficiency
- Too High : Hot Combustion Products Tend to Blow Out

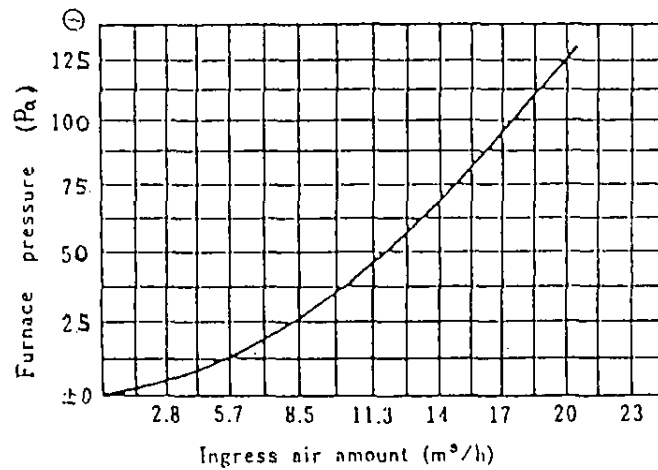
## ◆ Furnace Design Aspect

- Effective Furnace Length and Shape
- Application of Ceramic Fiber to Furnace Wall



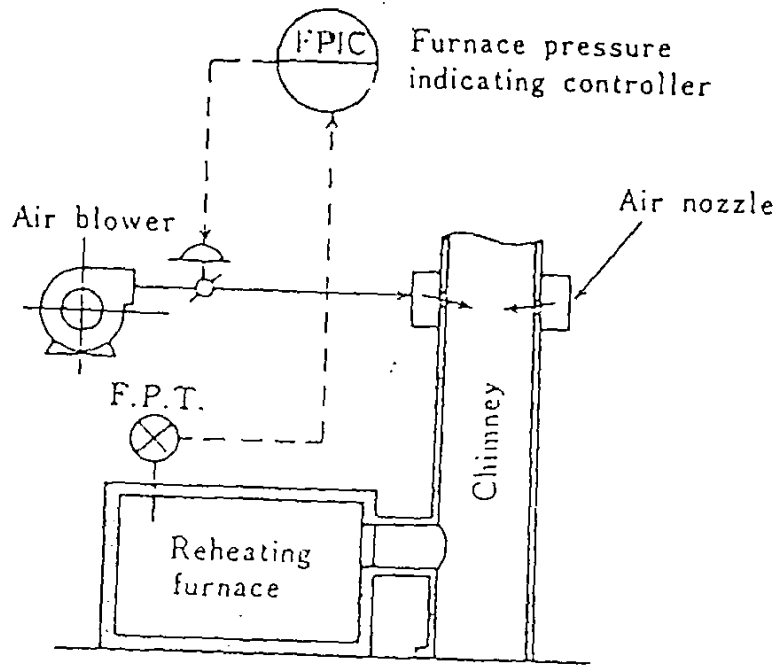


## Air Ingress during Reheating Furnace Operation

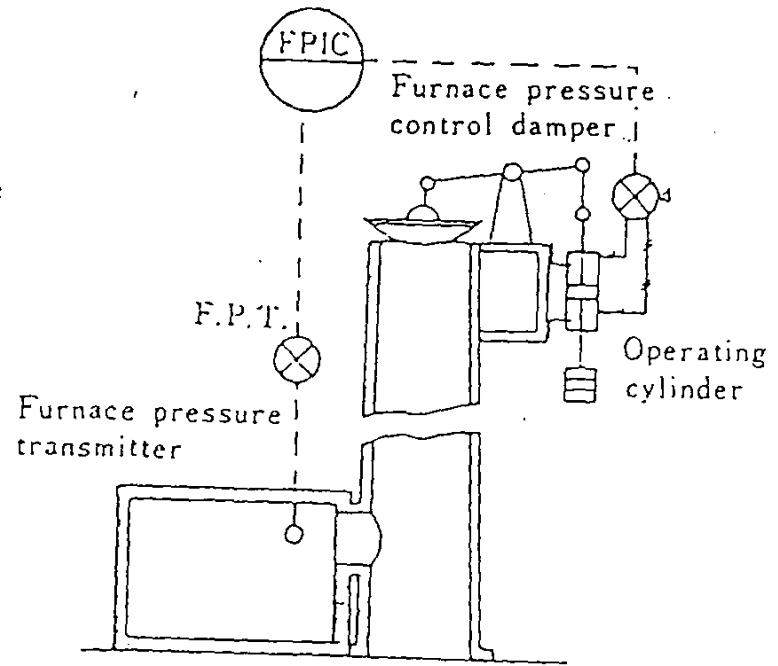


(Air ingress through 25.4mm square opening)

## Furnace Pressure vs Ingress Air Amount

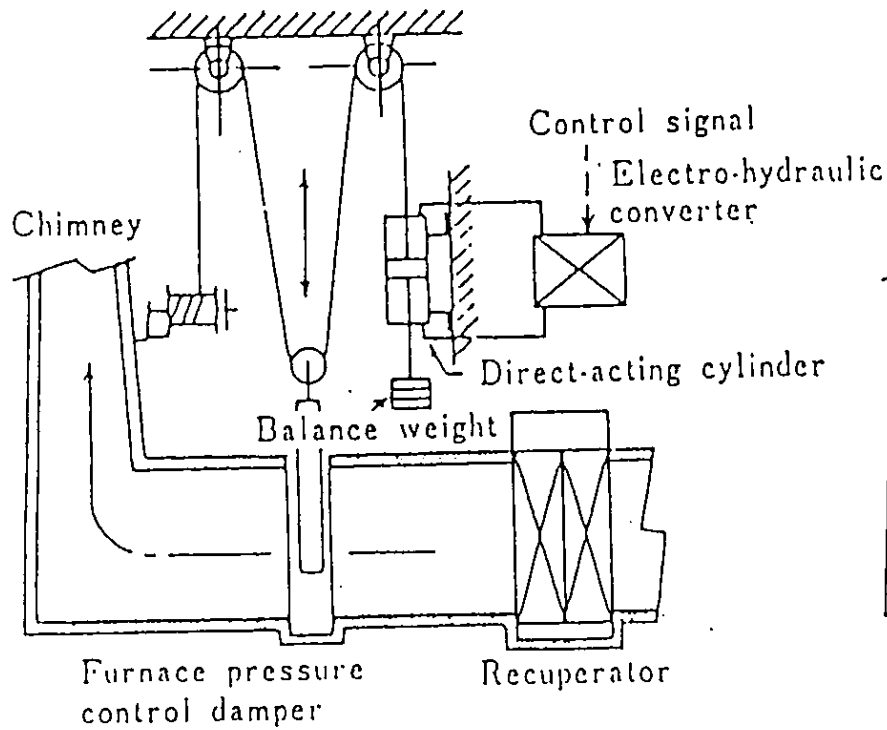


(a) Air curtain type

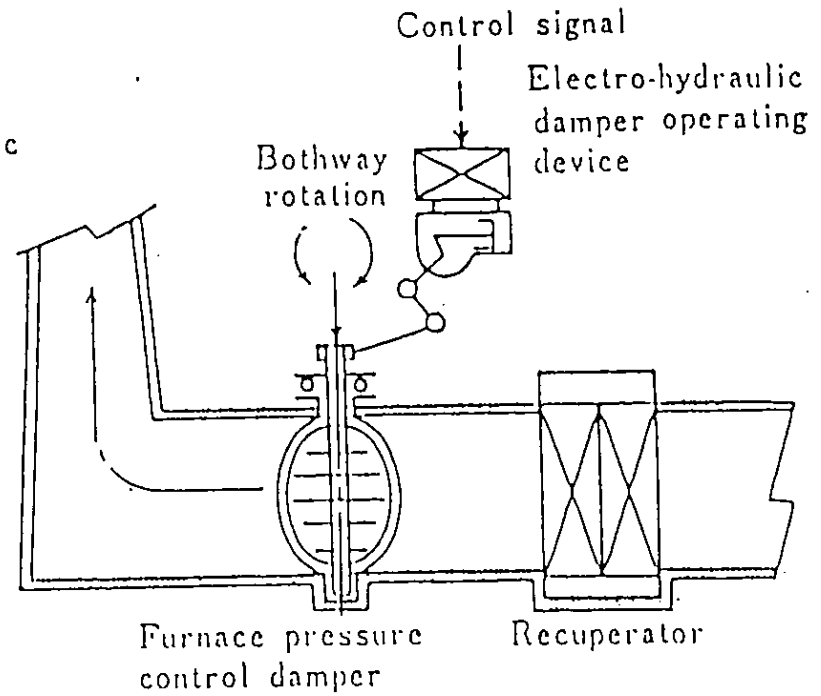


(b) Poppet valve type

# Damper for Pressure Control



(a) Suspended slide damper



(b) Rotary (butterfly) type damper

# Damper Configuration



# Case Study of ECCJ Factory

## How to Save Energy

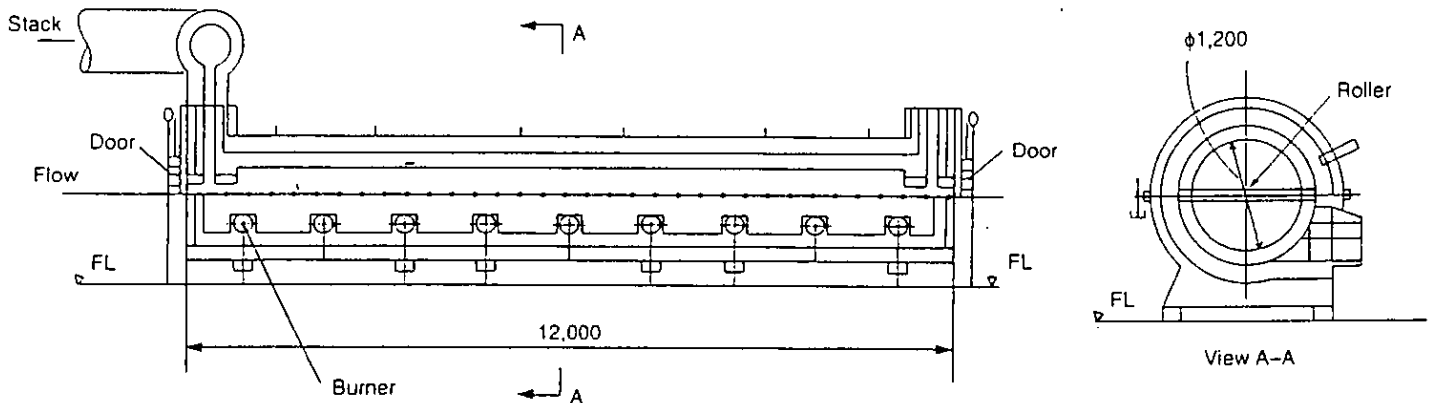
- ◆ Excess Air Reduction
  - Install Flow Control System
- ◆ Wall Heat Loss Reduction
  - Enhance Heat Insulation of Furnace Wall
- ◆ Exhaust Gas Heat Loss Reduction
  - Install Heat Exchanger at Chimney
- ◆ Combination of Above Three Improvements



# Heating Furnace

1) Type Roller Hearth Type Bar Heating Furnace for Quenching

2) Dimension



3) Capacity		1000 kg/h
4) Fuel	Heating Varyu of Heavy A Oil	42.11 MJ/kg
	Theoretical Air Requirement	11.09 m <sup>3</sup> N/kg
	Quantity of the Waste Gas (Air Ratio = 1)	11.82 m <sup>3</sup> N/kg
5) Fuel Consumption		61.315kg/h
6) Combustion Air Temp.		33°C
7) Fuel Temp.		33°C
8) Air Ratio		1.6
9) NOx in Exhaust Gas		250 ppm
10) Waste Gas Temp.		1000°C
11) Furnace Wall Temp.		1000°C
12) Material Temp.		33°C → 950°C
13) Surface Temp. of Body	Cylindrical Wall	134°C
	Vertical Wall	135°C
14) Furnace Wall Structure	Fire Brick SK33	115 mm
	Insulating Brick B6	115 mm
15) Cooling Water Heat Loss		2m <sup>3</sup> /h 30°C → 40°C
16) Furnace Pressure		49 Pa
17) Generated Scale		7 kg/ton of Raw Material
18) Average Specific Heat at Constant Pressure	Air	1.298 kJ/m <sup>3</sup> N°C
	Waste Gas	1.381 kJ/m <sup>3</sup> N°C
	Iron	0.699 kJ/kg°C
	Scale	0.900 kJ/kg°C
19) Heat of Oxidizing Reaction (Fe)		5.588 MJ/kg
20) Total Fe in Scale		0.755
	Air ratio could be reduced to 1.2.	
	Scale loss at air ratio 1.2 would be 70% of that at air ratio 1.6.	
21) Burner Type		Compressed Air Atomizing Burner

This furnace, called the roller furnace, is used for increasing the strength of steel rods by continuously quenching and hardening.

A simple specification is shown in the attached sheets. Steel rods are cut into a prescribed size, inserted in succession from the furnace inlet, and heated to 950°C. The heating capacity is 1000kg/h, and A heavy oil is used as fuel.

Contents of this heavy oil are shown below. The low heating value, theoretic excess air ratio and theoretic exhaust gas quantity are given here, but these can be easily calculated as follows.

#### A Heavy Oil

Contact      C; 86%          H; 13%          S; 0.1%          O; 0.7%  
                   N; 0.03%

#### Equation

$$\begin{aligned} & \text{A Heavy Oil (1 kg); } \frac{0.86}{12} \text{C} + \frac{0.13}{1} \text{H} + \frac{0.001}{32} \text{S} + \frac{0.007}{16} \text{O} + x\text{O}_2 \\ \rightarrow & \frac{0.86}{12} \text{CO}_2 + \frac{0.13}{2} \text{H}_2\text{O} + \frac{0.005}{32} \text{SO}_2 \\ x = & \frac{0.86}{12} + \frac{0.13}{2 \times 2} + \frac{0.001}{32} - \frac{0.007}{32} = 0.1040 \\ & 0.1040 \times 22.4 = 2.330 \text{ Nm}^3/\text{kg fuel} \end{aligned}$$

- 1)  $A_0 = 2.330/0.21 = 11.09 \text{ Nm}^3/\text{kg fuel}$
- 2)  $G_0 = \left( \frac{0.86}{12} + \frac{0.13}{2} + \frac{0.001}{32} + \frac{0.0003}{28} \right) \times 22.4 + 11.09 \times 0.79$   
 $= 11.82 \text{ Nm}^3/\text{kg fuel}$
- 3)  $H_1 = 42.11 \text{ MJ/kg}$

For combustion, while the fuel is ON-OFF controlled so that the wall temperature is 1000°C at the furnace center, the average excess air ratio is very high as 1.6 because the air flows in even during the OFF time.

The exhaust gas, at 1000°C, is discharged from the gas duct provided before the furnace inlet. When calculating a heat value that the exhaust gas takes, as shown in Table 3.9, the exhaust gas's specific heat varies by gas content and temperature. Strictly speaking, it needs to be calculated for each case.

However, here it is calculated based on 1.381 KJ/m<sup>3</sup>N°C and constant.

The heat insulation configuration is firebrick SK33 115 mm + insulating firebrick B6

115 mm. Their mean heat conductivity and the furnace's outside and inside surface temperature are also shown in the chapter of insulation including examples of energy conservation type. Strictly, the heat conductivity is also a function of temperature, and porous materials have more of this tendency. However, here it is also considered as a constant.

This furnace is cylinder shaped. When calculating a heat loss from furnace wall, the heat transfer calculation is conducted using formulas applicable to the cylinder. Additionally, heat loss at the inlet and outlet are calculated using formulas for plane boards. However, here you may use the value which already calculated.

A furnace inevitably has openings including the inlet and outlet, however, radiation loss, air invasion and blow out of furnace gas from these openings should be avoided as much as possible. These factors can be calculated by the area of opening, wall thickness and furnace pressure.

Invasion of air and blow out of furnace gas, in particular, should be given consideration when examining whether to provide a damper control or not. However, here these are considered as negligibly small compared with other heat losses.

Scale production largely depends on the furnace temperature and the oxygen concentration of furnace gas.

Reduction of excess air ratio is the first to be considered in terms of energy conservation. In conducting the present calculation, it is assumed that the excess air ratio can be reduced to 1.2. And, in this case, scale production is supposed to be 70%.

In case of iron the produced scale consists of  $\text{FeO}$ ,  $\text{Fe}_3\text{O}_4$  and  $\text{Fe}_2\text{O}_3$  and for each the producing heat and specific heat are different. However, if a scale analysis is not conducted, it is specified in the JIS that the producing heat may be supposed to be 5.588 MJ/kg, the specific heat 0.90 KJ/kg $^{\circ}\text{C}$ , and the iron content in scale as 75.5%.

The specific heat of steel varies itself by temperature. Especially, as the steel involves phase transformation, the specific heat increases a lot near the phase transformation. Thus, while a table of specific enthalpy as shown in Table 5.1 should be used for strictness in cases of heating exceeding the phase transformation point of 727 $^{\circ}\text{C}$ , here 0.699 KJ/kg $^{\circ}\text{C}$  is taken as a mean specific heat.

Using these values, heat balance of the current furnace is calculated as the attached sheets.

Next, to examine effects of various energy saving measures to this furnace, heat balance is calculated for each. As measures first to be applied, reduction of excess air ratio, enhancement of heat insulation, recovery of exhaust heat, etc. are considered, and each follows premises as shown below.

Excess air ratio is reduced from 1.6 to 1.2, heat insulation is enhanced by veneering the furnace's inner surface with ceramic fiber, and combustion air is preheated to 600 $^{\circ}\text{C}$  by heat recovery.

Since the fuel consumption  $X$  is unknown, first it is determined based on an assumption that the input heat equals the output heat, and the value is substituted for further calculation.

As an example, the result of simultaneously applying all measures is shown. To examine the contribution of each measure, results of individual measures are to be calculated by yourself.

Combinations to be examined are the following.

1. excess air reduction (auto combustion system)
2. heat insulation enhancement
3. heat recovery
4. combination of above 1., 2., and 3.

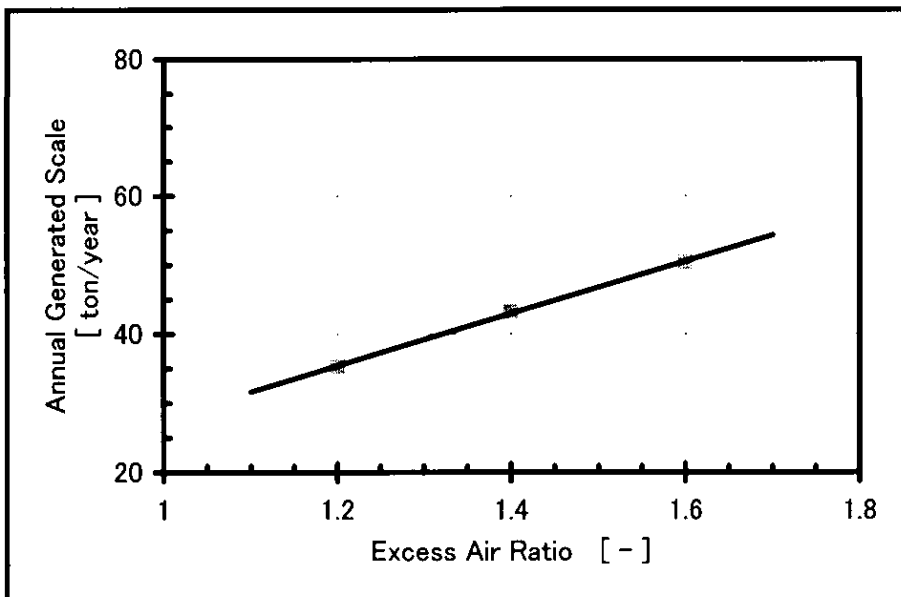
Veneering Thickness (mm)	0 (Existing)	25	50	75	100
Surface Tem. Cylindrical Wall (°C)	134	113	100	90	82
Surface Tem. Vertical Wall (°C)	135	118	106	97	91
Wall Heat Loss Cylindrical Wall (MJ/h)	356.9	262.8	206.2	168.5	141.5
Wall Heat Loss Vertical Wall (MJ/h)	14.4	11.3	9.3	7.9	6.9
Total Heat Loss (MJ/h)	371.3	274.1	215.5	176.4	148.4

**Table 8. Wall Loss as Function of Veneering Thickness**

## Scale Loss Improvement

Excess Air Ratio	Generated Scale	Annual Generated Scale
-	kg/ton	ton/year
1.6	7.0	50.4
1.4	6.0	43.2
1.2	4.9	35.3

Heating Furnace Operation Hour : 7200 h/year



## Heat Balance of the Current Furnace

### Input Heat Total 2612 MJ/h

#### 1) Fuel's Heat Value 2582.00 MJ/h

$$\begin{array}{l} \text{Fuel Consumption} \qquad \qquad \text{Low Calorific Value} \\ 61.3154 \text{ kg/h} \quad * \quad 42.11 \text{ MJ/kg} \end{array}$$

#### 2) Scale's Producing Heat 29.53 MJ/h

$$\begin{array}{l} \text{Generated Scale} \qquad \qquad \text{Capacity} \\ 7 \text{ kg/ton} * 0.755 * 1.0 \text{ ton/h} * 5.588 \text{ MJ/kg} \\ \text{Total Fe in Scale} \qquad \qquad \text{Heat of Oxidizing Reaction (Fe)} \end{array}$$

### Output Heat Total 2612 MJ/h

#### 3) Material's Sensible Heat 637.65 MJ/h

$$\begin{array}{l} \text{Capacity} \qquad \qquad \text{Generated Scale} \qquad \qquad \text{Material Temp.} \\ (1000 \text{ kg/h} - 0.755 * 7 \text{ kg/h}) * 0.699 \text{ kJ/kg}^\circ\text{C} * (950^\circ\text{C} - 33^\circ\text{C}) \\ \text{Total Fe in Scale} \qquad \qquad \text{Specific Heat of Iron} \end{array}$$

#### 4) Exhaust Gas Loss 1513.11 MJ/h

$$\begin{array}{l} \text{Specific Heat of Waste Gas} \qquad \qquad \text{Fuel Consumption} \\ 1.381 \text{ kJ/m}^3\text{N}^\circ\text{C} * 18.474 \text{ m}^3\text{N/kg} * 61.3154 \text{ kg/h} * (1000^\circ\text{C} - 33^\circ\text{C}) \\ \text{Waste Gas Quantity} \qquad \qquad \qquad \text{Waste Gas Temp.} \\ \\ \text{Waste Gas Quantity} \qquad \qquad \text{Theoretical Air Quantity} \\ 18.474 \text{ m}^3\text{N/kg} = 11.82 \text{ m}^3\text{N/kg} + 11.09 \text{ m}^3\text{N/kg} * (1.6 - 1.0) \\ \text{Theoretical Waste Gas Quantity} \qquad \qquad \text{Excess Air} \end{array}$$

#### 5) Radiation Heat Loss from Furnace Wall 371.34 MJ/h

$$\begin{array}{l} \text{Heat Loss from Cylindrical Wall} \\ 356.90 \text{ MJ/h} + 14.44 \text{ MJ/h} \\ \text{Heat Loss from Vertical Wall} \end{array}$$

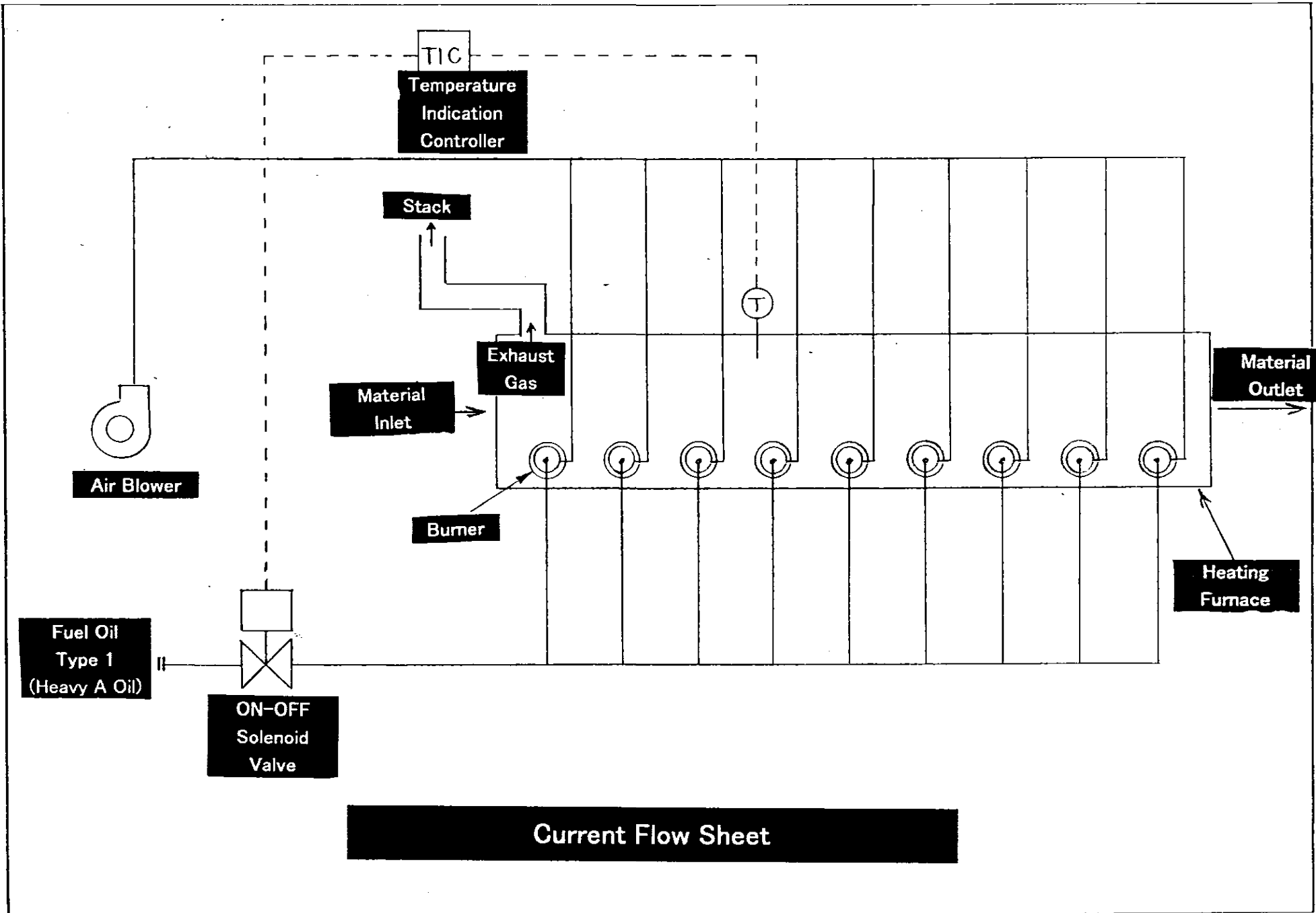
#### 6) Heat taken by Cooling Water 83.72 MJ/h

$$\begin{array}{l} \text{Specific Heat of Water} \qquad \qquad \text{Cooling Water Quantity.} \\ 4.186 \text{ MJ/m}^3\text{N}^\circ\text{C} * (40 - 30) * 2 \text{ m}^3\text{N/h} \\ \text{Cooling Water Temp.} \end{array}$$

#### 7) Scale's Sensible Heat 5.78 MJ/h

$$\begin{array}{l} \text{Specific Heat of Scale} \qquad \qquad \text{Material Temp.} \\ 0.900 \text{ kJ/kg}^\circ\text{C} * 7 \text{ kg/h} * (950^\circ\text{C} - 33^\circ\text{C}) \\ \text{Generated Scale} \end{array}$$





**Price List of Improved Equipment and Other Related Items for Heating Furnace**

Improved Equipment Name	Specifications	Price US\$ (Including Laborage)
1. Automatic Combustion Control Equipment (Including Damper Control)	Temperature Control Flow Rate Control Automatic Valve	32000
2. Thermal Insulation Material	Ceramic Fiber      25mm Plywood Ring      50mm 75mm 100mm	16600 23800 33300 40400
3. Waste Heat Recovery Collecting System 1 (Large Size)	Recuperator Max. Exhaust Gas Volume 1100 m <sup>3</sup> N/h Max. Air Volume 1000 m <sup>3</sup> N/h Exhaust Gas Intake Temp. 800°C Air Outlet Temp. 650°C Air Duct Thermal Insulation	120000
4. Waste Heat Recovery Collecting System 2 (Small Size)	Recuperator Max. Exhaust Gas Volume 500 m <sup>3</sup> N/h Max. Air Volume 450 m <sup>3</sup> N/h Exhaust Gas Intake Temp. 800°C Air Outlet Temp. 650°C Air Duct Thermal Insulation	50000